

**Argonne National Laboratory**

**MOMENTS OF FIRST-PASSAGE DISTRIBUTIONS  
IN SLAB GEOMETRY**

**by**

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## I. INTRODUCTION

There exists a variety of physical processes having a Markovian character in which a particle suffers a succession of independent collisions with atoms of the medium through which it travels. Examples are the following: the diffuse scattering of light, where the particle is a photon; the diffusion of neutrons; the multiple scattering of charged particles. In connection with such processes, one is often interested in the probability distribution of the state variables of the particles (position, velocity, wavelength, spin, etc.) when they make first passages through some surface in space (regardless of the times of emergence). A general stochastic theory of such first-passage distributions has been developed by Moyal,<sup>10,11</sup> and Brockwell.<sup>3</sup> For a comprehensive account of the theory of branching processes as applied to neutron transport theory, we refer the reader to Mullikin.<sup>13</sup>

The following specific transport model will be dealt with in this report. We shall be concerned with a population of particles (for example, neutrons), the state of an individual particle being represented by a vector  $\underline{y} = (\underline{x}, \underline{\mu})$ , where  $\underline{x}$  denotes position and  $\underline{\mu}$  denotes direction of motion. (Particle speed is assumed to be essentially constant—this is the classical one-group approximation.) We denote by  $Y$  the set of all possible individual states and by  $\mathcal{B}(Y)$  the Borel field of subsets of  $Y$ . The population state space  $\mathcal{V}$  is then defined by

$$\mathcal{V} = \bigcup_{n=0}^{\infty} Y^n,$$

where  $Y^n$ ,  $n \geq 1$ , denotes the  $n$ -fold Cartesian product of  $Y$  with itself, and  $Y^0$  denotes the state in which the population is empty. Measurable subsets of  $\mathcal{V}$  are defined to be those belonging to the  $\sigma$ -field  $\mathcal{B}(\mathcal{V})$  generated by the product  $\sigma$ -fields  $\mathcal{B}(Y^n)$ ,  $n = 0, 1, 2, \dots$ . A typical element of  $\mathcal{V}$  corresponding to a population of size  $n$  will be denoted by  $\underline{y}^{(n)}$ . (We imagine the particles to be labeled in some way so that  $\underline{y}^{(n)}$  is an ordered  $n$ -tuple.) For a detailed account of the theory of stochastic population processes, see Moyal.<sup>9</sup>

We suppose that the behavior of the population of particles is governed by the following functions (which we assume known from quantum-mechanical or other considerations):

1. The total cross section or inverse mean-free-path,  $\lambda(\underline{x})$

Given a particle with state  $\underline{y} = (\underline{x}, \underline{\mu})$ , the probability that it experiences a collision in traveling a small distance  $d\ell$  is  $\lambda(\underline{x})d\ell + o(d\ell)$ . The probability of more than one collision in  $d\ell$  is  $o(d\ell)$ .

2. The collision outcome distribution,  $\{\phi_n\}$

The distribution  $\{\phi_n\}$  is a conditional probability measure on  $\mathcal{B}(Y) \times Y$ . More specifically,  $\phi_n(A|\underline{y})$  is the probability, given that a particle with state  $\underline{y}$  experiences a collision, that exactly  $n$  particles are produced with states  $\underline{y}_1, \dots, \underline{y}_n$  such that  $\underline{y}^{(n)} = (\underline{y}_1, \dots, \underline{y}_n) \in A$ . Note that the colliding particle itself (if it survives the collision) is included among the particles produced. For photon scattering, where only absorption or scattering are possible,  $\phi_n = 0$  for  $n \geq 2$ . In general,

$$\sum_{n=1}^{\infty} \phi_n(Y^n|\underline{y}) = 1 - \phi_0(\underline{y}),$$

where  $\phi_0(\underline{y})$  is the probability that the colliding particle is absorbed.

In addition to assuming that  $\lambda$  and  $\{\phi_n\}$  are known, we assume that between collisions each particle experiences a change in position only (i.e.,  $\underline{\mu}$  is constant). Moreover, we suppose that there is no interaction between the particles themselves, only between the particles and the atoms of the medium through which they move.

The problems we shall discuss here fall into the general class of first-passage problems (see Moyal<sup>10</sup>). Given a single initial particle in a slab of thickness  $t$  (infinite in two directions), we specify its position by a single coordinate  $x$  ( $0 \leq x \leq t$ ) and its direction of motion by the cosine  $\mu$  of the angle it makes with the positive  $x$ -axis (normal to the slab faces). The problem can be stated as follows: Given a single initial particle with state  $\underline{y} = (x, \mu)$ , what is the probability distribution of the resulting population of particles making first passages from the slab (the state of each particle in this population being its state as it emerges from the slab)? If the exterior of the slab is vacuous (so that returns to the slab are impossible), then the first-passage population is identical with the total emergent population. We shall use the terms emergent population and first-passage population interchangeably.

For an arbitrary convex body with surface  $\Sigma$ , the number of particles making first passages from the body is a random number  $n$ , and the states of the emerging particles can be represented by an element  $\underline{y}^{(n)} = (y_1, \dots, y_n)$  of the population state space  $\mathcal{Y}$ . It is useful to introduce the generating functional (conditional on a single initial particle with state  $\underline{y}$ )

$$\begin{aligned} G(\xi | \underline{y}) &= E \xi(y_1) \xi(y_2) \dots \xi(y_n) \\ &\equiv P_0(\underline{y}) + \sum_{n=1}^{\infty} \int_{\mathcal{Y}^n} \dots \int \xi(y_1) \dots \xi(y_n) P_n(d\underline{y}_1 \dots d\underline{y}_n | \underline{y}), \end{aligned}$$

where  $\xi$  is an arbitrary measurable function on  $\mathcal{Y}$  such that

$$\sup_{\underline{y} \in \mathcal{Y}} |\xi(\underline{y})| \leq 1$$

and  $P_n(A | \underline{y})$  is the probability, given a single initial particle with state  $\underline{y}$ , that the state  $\underline{y}^{(n)}$  of the first-passage population satisfies  $\underline{y}^{(n)} \in A$ . We then obtain the following stochastic form of the Boltzmann equation (see, for example, Moyal,<sup>11</sup> Pál,<sup>14</sup> Bell,<sup>2</sup> and Brockwell<sup>4</sup>):

$$[\underline{\mu} \cdot \nabla - \lambda(\underline{x})] G(\xi | \underline{y}) = -\lambda(\underline{x}) \left[ \phi_0(\underline{y}) + \sum_{n=1}^{\infty} \int_{\mathcal{Y}^n} \dots \int \phi_n(d\underline{y}_1 \dots d\underline{y}_n | \underline{y}) \prod_{i=1}^n G(\xi | \underline{y}_i) \right], \quad (1)$$

with boundary conditions

$$\begin{aligned} G(\xi | \underline{y}) &= \xi(\underline{y}) \text{ if } \underline{x} \text{ is on the surface } \Sigma \\ &\text{and } \underline{\mu} \text{ is directed outwards,} \end{aligned} \quad (2)$$

where  $\underline{y} = (\underline{x}, \underline{\mu})$ .

The generating functional  $G$  uniquely determines (see Moyal<sup>9</sup>) a symmetric distribution on the measurable space  $(\mathcal{Y}, \mathcal{B}(\mathcal{Y}))$ , which is just the probability distribution of the first-passage population. However, the equation for  $G$  is difficult to solve because of its nonlinearity. Instead, we shall study the associated moment distributions for which the Boltzmann equation is linear.

We shall assume that  $\phi_n$ ,  $n = 1, 2, \dots$ , takes the form

$$\phi_n(d\underline{y}_1 \dots d\underline{y}_n | \underline{y}) = \Pi_n \left[ \prod_{i=1}^n \delta(\underline{x}_i - \underline{x}) \phi(d\underline{\mu}_i | \underline{\mu}) d\underline{x}_i \right], \quad (3)$$

where  $\Pi_n$  is the probability that exactly  $n$  particles result from the collision,  $\delta$  is the three-dimensional Dirac delta function, and  $\phi(d\mathcal{V}|\mu)$  is the probability that a particle produced by the collision has a direction of motion in the element of solid angle  $d\mathcal{V}$  about  $\mathcal{V}$ . In subsequent sections, we will assume that  $\phi(d\mathcal{V}|\mu)$  is of the form

$$\phi(d\mathcal{V}|\mu) = \sigma(\theta) d\mathcal{V}, \quad (4)$$

where  $\theta$  is the angle between  $\underline{\mu}$  and  $\mathcal{V}$ , and that the absorption probability  $\phi_0(\mathcal{V})$  is constant (equal to  $\Pi_0$ ).

The analysis will be confined to slab geometry, so that the state  $\mathcal{Y}$  will be represented by a pair of scalars  $(x, \mu)$  and  $\lambda$  will be a function of  $x$  only. By a simple scale transformation, we may assume without loss of generality that  $\lambda$  is constant.

In this report, we shall use the discrete approximation method developed by Brockwell<sup>3</sup> to derive the equations giving the first two moments of the joint first-passage distribution for the model described above. That is, equations will be given for the means, variances, and covariances of the numbers of particles emerging with various states from the slab, conditional on a single initial particle in the slab with given initial state. In addition to calculating solutions of these equations, we shall also use them to estimate the critical length of the slab, i.e., the smallest length for which the mean number of emergent particles becomes infinite. (This is one of the many possible definitions of critical length. For a discussion of the relationship between the various definitions, see Moyal<sup>11</sup> and Brockwell and Moyal.<sup>5</sup>)

The discrete approximation we shall use in the analysis is presented in Section II.

The development of the equations for the first two moments and the solutions of these equations are given in Section III.

A computer program was written to calculate the solutions, and the results are given for a variety of different collision outcome distributions in Section IV. The appendix gives in detail the mathematical methods used in the computer code to solve the equations.

## II. THE BASIS OF THE DISCRETE APPROXIMATION

The icosahedral approximation developed by Brockwell<sup>3</sup> is used. A complete discussion of this approximation is given in Chapter VI of Ref. 3, so only a summary is given here. We are concerned with scattering, absorption, and fission in a plane slab, infinite in two directions and with finite thickness  $t$ .

The state of any particle is determined by its position and direction of motion. (We consider only the case of particles with a single energy, i.e., the one-group case, although there is no conceptual difficulty in the generalization involving multiple energies. In fact, H. Greenspan (of the ANL Applied Mathematics Division) is currently working on a computer program using analogs of the equations developed in Section III for particles with a finite set of possible energies. His results will provide the first- and second-moment structure for the more realistic case in which the dependence of  $\lambda$  and  $\{\phi_n\}$  on energy, or other additional state variables, is taken into account.) The position of any particle is specified by its distance  $x$  ( $0 \leq x \leq t$ ) from the left face of the slab. It is in the specification of the direction of motion that the icosahedral approximation enters.

The essential approximation to the model described in Section I is the following: The directions of motion of each particle are constrained to a set of 30 unit vectors corresponding to points evenly spaced on the surface of the unit sphere. That is, a particle may not travel in an arbitrary direction, but only in directions represented by these 30 unit vectors.

The 30 vectors are chosen in the following way: A regular icosahedron is oriented as in Fig. 1 so that the line joining its center to the midpoint of one edge is in the direction of the unit vector  $\hat{i}$  normal to the slab faces (and in the direction of increasing  $x$ ).

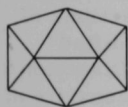


Fig. 1. Orientation of the Icosahedron

The 30 possible directions of motion are then taken to be along the lines joining the center of the icosahedron to the midpoints of its edges. If we let  $\{\hat{a}_1, \dots, \hat{a}_{30}\}$  be the unit vectors in these directions, then the set of scalar products  $\{\hat{a}_i \cdot \hat{a}_1, \hat{a}_i \cdot \hat{a}_2, \dots, \hat{a}_i \cdot \hat{a}_{30}\}$  gives the cosines of the possible angular deflections for a particle initially traveling in direction  $\hat{a}_i$ . This (unordered)

set is the same for each  $i$  ( $i = 1, \dots, 30$ ). This means that for any direction of motion before a collision, the set of all possible angular deflections resulting from the collision is the same, independent of the initial direction of motion; that is, we can define a single set of 30 possible angular deflections  $\{\epsilon_1, \dots, \epsilon_{30}\}$  which take an arbitrary initial direction  $\hat{a}_i$  into the set  $\{\hat{a}_1, \dots, \hat{a}_{30}\}$  of all possible directions of motion. This set  $\{\epsilon_1, \dots, \epsilon_{30}\}$  contains only nine distinct angles  $\theta_1, \dots, \theta_9$ , where

$$\begin{aligned} \cos \theta_1 &= \mu_1, & \cos \theta_9 &= -\mu_1, \\ \cos \theta_2 &= \mu_2, & \cos \theta_8 &= -\mu_2, \\ \cos \theta_3 &= \mu_3, & \cos \theta_7 &= -\mu_3, \\ \cos \theta_4 &= \mu_4, & \cos \theta_6 &= -\mu_4, \\ \cos \theta_5 &= \mu_5, \end{aligned}$$

(5)



and

$$\begin{aligned}
 \mu_1 &= 1 & = -\mu_{10}, \\
 \mu_2 &= \frac{1}{4}(1 + \sqrt{5}) & = -\mu_9, \\
 \mu_3 &= \frac{1}{2} & = -\mu_8, \\
 \mu_4 &= \frac{1}{4}(\sqrt{5} - 1) & = -\mu_7, \\
 \mu_5 &= 0 & = -\mu_6.
 \end{aligned} \tag{6}$$

The angles  $\theta_2, \theta_3, \dots, \theta_8$  each occur four times in the set  $\{\epsilon_1, \dots, \epsilon_{30}\}$ . Assuming that the probability of a deflection through angle  $\theta$  depends only on  $\theta$ , we need therefore define only nine distinct transition probabilities  $\{p_1, 4p_2, \dots, 4p_8, p_9\}$  corresponding to angular deflections  $\{\theta_1, \theta_2, \dots, \theta_9\}$ . The problem of determining the  $p_i$ 's from the distribution  $\phi(d\vartheta|\mu)$  defined in Eq. 3 is considered later in this section.

With the orientation of the icosahedron defined above, the cosines of the angles between the 30 vectors representing possible directions of motion and the positive x-axis take only nine distinct values,  $\mu_1, \dots, \mu_5 (= \mu_6), \mu_7, \dots, \mu_{10}$ , where the  $\mu_i$ 's are defined in Eq. 6. Considerable simplification can therefore be achieved by grouping the directions of motion according to the cosine of the angle they make with the positive x-axis. The number  $\alpha (\alpha = 1, \dots, 10)$  will be used to denote the set of all directions of motion whose direction cosine is  $\mu_\alpha$ . The definition must be modified slightly for the directions 5 and 6 perpendicular to the x-axis. Direction 5 consists (see Fig. 1) of the two unit vectors  $\pm \mathbf{k}$ , and direction 6 consists of the unit vectors  $\pm \mathbf{j}$ . This splitting of the directions perpendicular to the x-axis is necessary so that the process, when defined in terms of the state variables  $(x, \alpha)$ , be Markovian. We say that a particle has state  $(x, \alpha)$  if its distance from the left end of the slab is  $x$  ( $0 \leq x \leq t$ ), and the cosine of its direction of motion is  $\mu_\alpha$  ( $\alpha = 1, \dots, 10$ ).

In practice, of course, the particle can move in any direction in space. When a particle makes a collision with an atom of the slab, it gives rise to a random number ( $n = 0, 1, 2, \dots$ ) of particles of the same type. As described in Eq. 3, we shall assume that, conditional on a particle with direction  $\mu$  experiencing a collision and giving rise to  $n$  particles ( $n \geq 1$ ), the directions of motion of the resulting particles are independently and identically distributed with distribution  $\phi(d\vartheta|\mu)$ , where

$$\phi(d\vartheta|\mu) = \sigma(\theta) d\vartheta, \tag{7}$$

$\theta$  is the angle between  $\vartheta$  and  $\mu$ , and  $d\vartheta$  is an element of solid angle surrounding the unit vector  $\vartheta$ . We must determine  $p_1, \dots, p_9$  corresponding to the continuous function  $\sigma(\theta)$ . Since the original vectors  $\{\mathbf{a}_1, \dots, \mathbf{a}_{30}\}$  each

correspond to congruent regions of the unit sphere, the probabilities are chosen so that

$$p_i = k\sigma(\theta_i), \quad i = 1, \dots, 9, \quad (8)$$

the constant  $k$  being determined by the normalization condition,

$$p_1 + 4 \sum_{i=2}^8 p_i + p_9 = 1. \quad (9)$$

For example, if scattering is isotropic, then  $\sigma(\theta) = 1/(4\pi)$ , and Eqs. 8 and 9 give

$$p_1 = p_2 = \dots = p_9 = \frac{1}{30}.$$

If a particle with direction of motion  $i$  ( $i = 1, \dots, 10$ ) makes a collision that results in the production of  $n$  particles ( $n \geq 1$ ), then the directions of motion of the resulting particles are independently distributed, the distribution depending on the direction of motion of the colliding particle. This common distribution is specified (in the discrete model) by the probabilities

$$P_{ij} = \text{Prob} \{ \text{the resulting particle emerges from the collision with direction } j, \text{ given that the colliding particle was traveling in direction } i \text{ just before the collision} \}.$$

These probabilities must satisfy the normalization condition,

$$\sum_{j=1}^{10} P_{ij} = 1, \quad i = 1, \dots, 10. \quad (10)$$

The probabilities  $P_{ij}$  depend on which of the angular deflections  $\theta_1, \dots, \theta_9$  can bring about a transition from direction  $i$  to direction  $j$ , and this in turn depends on the geometry of the icosahedron. For example, a transition from direction 2 to direction 2 can occur by deflections through  $\theta_1, \theta_2, \theta_3$ , or  $\theta_4$ , and consequently  $P_{22} = p_1 + p_2 + p_3 + p_4$ . The other  $P_{ij}$ 's are found similarly and are shown below as the matrix  $P$  in which  $P_{ij}$  is the  $j$ th element of the  $i$ th row and the symbol  $(i_1, i_2, \dots, i_n)$  is used as an abbreviation for  $p_{i_1} + \dots + p_{i_n}$ .

$$P = \begin{bmatrix} (1) & (2222) & (3333) & (4444) & (55) & (55) & (6666) & (7777) & (8888) & (9) \\ (2) & (1234) & (2345) & (2356) & (46) & (37) & (4578) & (5678) & (6789) & (8) \\ (3) & (2345) & (1267) & (2457) & (28) & (46) & (3568) & (3489) & (5678) & (7) \\ (4) & (2356) & (2457) & (1368) & (37) & (28) & (2479) & (3568) & (4578) & (6) \\ (5) & (4466) & (2288) & (3377) & (19) & (55) & (3377) & (2288) & (4466) & (5) \\ (5) & (3377) & (4466) & (2288) & (55) & (19) & (2288) & (4466) & (3377) & (5) \\ (6) & (4578) & (3568) & (2479) & (37) & (28) & (1368) & (2457) & (2356) & (4) \\ (7) & (5678) & (3489) & (3568) & (28) & (46) & (2457) & (1267) & (2345) & (3) \\ (8) & (6789) & (5678) & (4578) & (46) & (37) & (2356) & (2345) & (1234) & (2) \\ (9) & (8888) & (7777) & (6666) & (55) & (55) & (4444) & (3333) & (2222) & (1) \end{bmatrix} \quad (11)$$

Note that each row contains  $p_1$  and  $p_9$  once and each of  $p_2, \dots, p_8$  four times. This is because each probability  $p_i$  corresponds to a particular unit vector representing the direction of motion of the particle after the collision, and, of the 30 possible unit vectors, exactly four correspond to each angular deflection  $\theta_2, \dots, \theta_8$ . Thus Condition 9 implies Condition 10.

### III. EQUATIONS FOR FIRST AND SECOND MOMENTS

In this section we develop the equations for the mean number of particles emerging in direction  $\alpha$  ( $\alpha = 1, \dots, 4, 7, \dots, 10$ ) conditional on an initial particle at position  $x$  ( $0 \leq x \leq t$ ) within the slab and traveling in direction  $\beta$  ( $\beta = 1, \dots, 10$ ). Particles cannot emerge traveling in direction 5 or 6, as these directions are parallel to the faces of the slab. The equations are also derived giving the variance-covariance structure of the number of particles emergent in direction  $\alpha_1$  and  $\alpha_2$  ( $\alpha_1 = 1, \dots, 4, 7, \dots, 10$ ;  $\alpha_2 = 1, \dots, 4, 7, \dots, 10$ ) conditional on a particle at position  $x$  ( $0 \leq x \leq t$ ) and traveling in direction  $\beta$  ( $\beta = 1, \dots, 10$ ). The solutions of these equations are then presented.

Denote by  $\underline{N} = (N_1, \dots, N_4, N_7, \dots, N_{10})$  the numbers of particles making first passages from the slab  $0 \leq x \leq t$  in directions 1, ..., 4, 7, ..., 10, respectively, and let  $P(\underline{N}|x, \nu)$  be the probability that  $\underline{N}$  particles make first passages from the slab conditional on a single initial particle with position  $x$  and direction cosine  $\nu$ . Similarly, let  $P(\underline{N}|x, \nu_1, \dots, \nu_k)$  denote the probability that  $\underline{N}$  particles make first passages conditional on  $k$  initial particles with position  $x$  and direction cosines  $\nu_1, \dots, \nu_k$  ( $-1 \leq \nu_i \leq 1$ ,  $i = 1, \dots, k$ ). It is convenient to introduce the generating functions

$$G(x, \nu) = \sum_{n_1, \dots, n_4, n_7, \dots, n_{10}=0}^{\infty} P(\underline{n}|x, \nu) z_1^{n_1} \dots z_4^{n_4} z_7^{n_7} \dots z_{10}^{n_{10}}, \quad |z_i| \leq 1,$$

and

$$G(x, \nu_1, \dots, \nu_k) = \sum_{n_1, \dots, n_4, n_7, \dots, n_{10}=0}^{\infty} P(n | x, \nu_1, \dots, \nu_k) z_1^{n_1} \dots z_4^{n_4} z_7^{n_7} \dots z_{10}^{n_{10}}, |z_i| \leq 1.$$

For clarity in writing  $G$ , we will suppress the arguments  $z_i$ . Then, since we are assuming that the particles do not interact with each other,

$$G(x, \nu_1, \dots, \nu_k) = G(x, \nu_1) \dots G(x, \nu_k).$$

The probability that a particle makes a collision in traveling a small distance  $\delta s$  is assumed to be  $\lambda \delta s + o(\delta s)$ , where  $\lambda$  is a positive constant. The probability of more than one collision is  $o(\delta x)$ . By measuring all distances in units of  $\lambda^{-1}$ , we can assume (without loss of generality) that  $\lambda = 1$ .

Given that a particle moving with direction cosine  $\nu$  experiences a collision, we assume that there is a probability  $\pi_0$  that the particle is absorbed and probabilities  $\pi_k(d\nu_1, \dots, d\nu_k | \nu)$ ,  $k = 1, 2, \dots$ , that  $k$  particles are produced with direction cosines in  $d\nu_1, \dots, d\nu_k$  ( $-1 \leq \nu_i \leq 1$ ). In the discrete model,  $\nu_i$  will take one of the values  $\mu_\alpha$ ,  $\alpha = 1, \dots, 10$ , with probability 1.

The initial particle will either experience no collisions before leaving the slab (in which case exactly one particle will emerge from the slab with direction cosine  $\nu$ , or the particle will experience a first collision at some point  $y$  within the slab. By considering these two possibilities, we obtain the first collision equation for  $G(x, \nu)$ :

$$G(x, \nu) = e^{-\nu^{-1}(t-x)} \prod_{\alpha=1, \dots, 4, 7, \dots, 10} z_\alpha^{\nu, \mu_\alpha} + \int_{y=x}^t \pi_0 e^{-\nu^{-1}(y-x)} \nu^{-1} dy \\ + \sum_{k=1}^{\infty} \int_{y=x}^t \int_{-1}^1 \dots \int_{-1}^1 \pi_k(d\nu_1, \dots, d\nu_k | \nu) G(y, \nu_1) \dots G(y, \nu_k) e^{-\nu^{-1}(y-x)} \nu^{-1} dy, \quad \text{if } \nu > 0, \quad (12)$$

$$G(x, \nu) = e^{\nu^{-1}x} \prod_{\alpha=1, \dots, 4, 7, \dots, 10} z_\alpha^{\nu, \mu_\alpha} + \int_{y=0}^x \pi_0 e^{-\nu^{-1}(y-x)} \nu^{-1} dy \\ + \sum_{k=1}^{\infty} \int_{y=0}^x \int_{-1}^1 \dots \int_{-1}^1 \pi_k(d\nu_1, \dots, d\nu_k | \nu) G(y, \nu_1) \dots G(y, \nu_k) e^{-\nu^{-1}(y-x)} \nu^{-1} dy, \quad \text{if } \nu < 0. \quad (13)$$

( $\delta_{\nu, \mu}$  is defined to be one if  $\nu = \mu$ , zero otherwise.) Differentiating Eqs. 12 and 13 with respect to  $x$ , we obtain the "backward" Kolmogorov equation,

$$\nu \frac{\partial}{\partial x} G(x, \nu) - G(x, \nu) = -\pi_0 - \sum_{k=1}^{\infty} \int_{-1}^1 \dots \int_{-1}^1 \pi_k(d\nu_1 \dots d\nu_k | \nu) G(x, \nu_1) \dots G(x, \nu_k), \quad (14)$$

with boundary conditions

$$G(x, \nu) = \prod_{\alpha=1, \dots, 4, 7, \dots, 10} z_{\alpha}^{\delta_{\nu, \mu_{\alpha}}} \quad \begin{array}{l} \text{if } x = 0 \text{ and } \nu < 0, \\ \text{or } x = t \text{ and } \nu > 0. \end{array} \quad (15)$$

(These equations are in fact a special case of Eqs. 1 and 2.)

We now make the further assumption (in accordance with Eq. 3) that the probability measures  $\pi_k$ ,  $k \geq 1$ , have the form

$$\pi_k(d\nu_1, \dots, d\nu_k | \nu) = \pi_k \pi(d\nu_1 | \nu) \pi(d\nu_2 | \nu) \dots \pi(d\nu_k | \nu), \quad (16)$$

where  $\pi_k$  is the probability that  $k$  particles are produced and

$$\int_{-1}^1 \pi(d\nu_1 | \nu) = 1.$$

The backward equation then becomes

$$\left[ \mu \frac{\partial}{\partial x} - 1 \right] G(x, \mu) = -\pi_0 - \sum_{k=1}^{\infty} \pi_k \left[ \int_{-1}^1 \pi(d\nu | \mu) G(x, \nu) \right]^k, \quad (17)$$

with the same boundary conditions as above.

Let  $M_{\alpha}(x, \mu)$  denote the expected number of particles emerging from the slab with direction  $\alpha$  (i.e., with direction cosine  $\mu_{\alpha}$ ),  $\alpha = 1, \dots, 4, 7, \dots, 10$ . Then, under the assumption that  $M_{\alpha}$  is bounded and

$$\sum_0^{\infty} k \pi_k = m < \infty,$$

we have

$$M_{\alpha}(x, \mu) = \left[ \frac{\partial}{\partial z_{\alpha}} G(x, \mu) \right]_{z_{\beta=1, \beta=1, \dots, 4, 7, \dots, 10}}. \quad (18)$$

Hence, from Eqs. 17 and 15,

$$\left[ \mu \frac{\partial}{\partial x} - 1 \right] M_{\alpha}(x, \mu) = -m \int_{-1}^1 \pi(d\nu | \mu) M_{\alpha}(x, \nu), \quad (19)$$

and

$$M_{\alpha}(x, \mu) = \delta_{\mu, \mu_{\alpha}} \quad \begin{array}{l} \text{if } x = 0 \text{ and } \mu < 0, \\ \text{or } x = t \text{ and } \mu > 0. \end{array} \quad (20)$$

(In deriving Eq. 19 from Eqs. 17 and 18, we have used the fact that

$$[G(x, \mu)]_{z_{\beta=1, \beta=1, \dots, 4, 7, \dots, 10}} = 1.$$

This follows from our assumption that  $M_{\alpha}$  is bounded.)

The second factorial moments of the numbers of emergent particles are obtained by a further differentiation of the generating function  $G$ . Thus, if we define

$$S_{\alpha\beta}(x, \mu) = \begin{cases} EN_{\alpha}N_{\beta} & \alpha \neq \beta \\ E[N_{\alpha}(N_{\alpha} - 1)] & \beta = \alpha \end{cases}$$

(assuming again that these moments are bounded), then

$$S_{\alpha\beta}(x, \mu) = \left[ \frac{\partial^2}{\partial z_{\alpha} \partial z_{\beta}} G(x, \mu) \right]_{z_1=\dots=z_4=z_7=\dots=z_{10}=1} \quad (21)$$

Provided

$$\sum_{k=0}^{\infty} k(k-1)\pi_k = m_{(2)} < \infty,$$

we then have, from Eqs. 15, 17, and 21,

$$\begin{aligned} \left[ \mu \frac{\partial}{\partial x} - 1 \right] S_{\alpha\beta}(x, \mu) &= -m \int_{-1}^1 \pi(d\nu | \mu) S_{\alpha\beta}(x, \nu) \\ &\quad - m_{(2)} \left\{ \int_{-1}^1 \pi(d\nu | \mu) M_{\alpha}(x, \nu) \right\} \left\{ \int_{-1}^1 \pi(d\nu | \mu) M_{\beta}(x, \nu) \right\}. \end{aligned} \quad (22)$$

and

$$S_{\alpha\beta}(x, \mu) = 0 \quad \begin{array}{l} \text{if } x = 0 \text{ and } \mu < 0, \\ \text{or } x = t \text{ and } \mu > 0. \end{array} \quad (23)$$

(Equations 22 and 23 are valid whether or not  $\alpha = \beta$ .)

So far we have not fully exploited our discrete approximation in deriving the equations for  $M_\alpha$  and  $S_{\alpha\beta}$ . In the discrete approximation, the initial direction  $\mu$  can take only one of the values  $\{\mu_1, \dots, \mu_{10}\}$  defined in Section II, and the integrals with respect to the measure  $\pi$  are in fact sums. Thus,

$$\int_{-1}^1 M_\alpha(x, \nu) \pi(d\nu | \mu_i) = \sum_{j=1}^{10} M_\alpha(x, \mu_j) P_{ij},$$

where  $P_{ij}$  is the probability that a particle produced at a collision travels in direction  $j$  conditional on the colliding particle traveling in direction  $i$  before the collision. Thus  $P_{ij}$  is the  $(i, j)$ th element of the matrix given in Eq. 11. Similarly,

$$\int_{-1}^1 S_{\alpha\beta}(x, \nu) \pi(d\nu | \mu_i) = \sum_{j=1}^{10} S_{\alpha\beta}(x, \mu_j) P_{ij}.$$

It is now convenient to change notation slightly. We write  $M_\alpha(x, i)$  for  $M_\alpha(x, \mu_i)$  ( $i = 1, \dots, 10$ ). Thus  $M_\alpha(x, i)$  is the mean number of particles emergent in direction  $\alpha$  ( $\alpha = 1, \dots, 4, 7, \dots, 10$ ), conditional on one particle at position  $x$  ( $0 \leq x \leq t$ ) traveling in direction  $i$ . The cosine of the angle between the direction of motion  $i$  and the positive  $x$ -axis is therefore  $\mu_i$ . Similarly, we write  $S_{\alpha\beta}(x, i)$  for  $S_{\alpha\beta}(x, \mu_i)$  ( $i = 1, \dots, 10$ ). Thus Eq. 19 may be written in matrix form,

$$\begin{bmatrix} \mu_1 \frac{\partial}{\partial x} - 1 & 0 \\ \vdots & \vdots \\ 0 & \mu_{10} \frac{\partial}{\partial x} - 1 \end{bmatrix} \begin{bmatrix} M_\alpha(x, 1) \\ \vdots \\ M_\alpha(x, 10) \end{bmatrix} = -m \begin{bmatrix} P_{11} & \dots & P_{110} \\ \vdots & & \vdots \\ P_{101} & & P_{1010} \end{bmatrix} \cdot \begin{bmatrix} M_\alpha(x, 1) \\ \vdots \\ M_\alpha(x, 10) \end{bmatrix}. \quad (24)$$

Since  $\mu_5 = \mu_6 = 0$ , we can write  $M_\alpha(x, 5)$  and  $M_\alpha(x, 6)$  as linear functions of  $M_\alpha(x, 1), \dots, M_\alpha(x, 4), M_\alpha(x, 7), \dots, M_\alpha(x, 10)$ . Doing this, and rearranging the terms, we may express Eq. 24 as

$$\frac{\partial}{\partial x} \begin{bmatrix} M_{\alpha}(x, 1) \\ \cdot \\ M_{\alpha}(x, 4) \\ M_{\alpha}(x, 7) \\ \cdot \\ M_{\alpha}(x, 10) \end{bmatrix} = R \begin{bmatrix} M_{\alpha}(x, 1) \\ \cdot \\ M_{\alpha}(x, 4) \\ M_{\alpha}(x, 7) \\ \cdot \\ M_{\alpha}(x, 10) \end{bmatrix}, \quad (25)$$

where  $R$  is an  $8 \times 8$  matrix which can be determined from Eq. 24. This is a system of eight homogeneous first-order linear differential equations, with boundary conditions given by Eq. 20. The solution is

$$\begin{bmatrix} M_{\alpha}(x, 1) \\ \cdot \\ M_{\alpha}(x, 4) \\ M_{\alpha}(x, 7) \\ \cdot \\ M_{\alpha}(x, 10) \end{bmatrix} = e^{Rx} \cdot \underline{c}, \quad (26)$$

where  $\exp(Rx)$  is the  $8 \times 8$  matrix defined as

$$\sum_{k=0}^{\infty} (Rx)^k / k!,$$

and  $\underline{c}$  is an eight-component column vector determined by the boundary conditions.

In fact, if we let  $M(x)$  be the  $8 \times 8$  matrix

$$\begin{bmatrix} M_1(x, 1) & \dots & M_4(x, 1)M_7(x, 1) & \dots & M_{10}(x, 1) \\ \cdot & & & & \cdot \\ \cdot & & & & \cdot \\ M_1(x, 4) & \dots & M_4(x, 4)M_7(x, 4) & \dots & M_{10}(x, 4) \\ M_1(x, 7) & \dots & M_4(x, 7)M_7(x, 7) & \dots & M_{10}(x, 7) \\ \cdot & & & & \cdot \\ \cdot & & & & \cdot \\ M_1(x, 10) & \dots & M_4(x, 10)M_7(x, 10) & \dots & M_{10}(x, 10) \end{bmatrix}, \quad (27)$$



then

$$M(x) = e^{Rx} \cdot C, \quad (28)$$

where  $C$  is an  $8 \times 8$  matrix determined by the boundary conditions. Using the boundary conditions for  $x = 0$  to get the lower half of  $C$ , and for  $x = t$  to get the upper half of  $M(t)$ , we have (by matrix partitioning)

$$\left[ \begin{array}{c|c} I & 0 \\ \hline A & B \end{array} \right] = \left[ \begin{array}{c|c} E_{11} & E_{12} \\ \hline E_{21} & E_{22} \end{array} \right] \cdot \left[ \begin{array}{c|c} C_1 & C_2 \\ \hline 0 & I \end{array} \right], \quad (29)$$

where

$$\left[ \begin{array}{c|c} E_{11} & E_{12} \\ \hline E_{21} & E_{22} \end{array} \right] = \exp(Rt),$$

and each of the indicated smaller matrices above is  $4 \times 4$ . Thus,  $C_1 = E_{11}^{-1}$  and  $C_2 = -E_{11}^{-1} \cdot E_{12}$ . Since  $M_\alpha(x, 5)$  and  $M_\alpha(x, 6)$  ( $\alpha = 1, \dots, 4, 7, \dots, 10$ ) can be expressed as linear functions of the terms in  $M(x)$ , the above gives a complete solution for the mean number of particles emergent in any of the eight possible emergent directions, conditional on one particle at an arbitrary position  $x$  within the slab, traveling in any of the 10 possible directions.

The above equations implicitly assume that the mean number of particles produced is finite. If the slab is supercritical, i.e., if the length of the slab is such that the mean of the total number of particles produced is infinite, then these equations will not be valid. However, this method may be used to determine the critical length for a given  $m$

$$\left( = \sum_{k=0}^{\infty} k\pi_k \right)$$

by varying the length  $t$  of the slab, and seeing for which value of  $t$  the total mean number of particles produced approaches infinity. This has been done, and the results are reported in Section IV.

To find the functions  $S_{\alpha\beta}$ , we now apply similar methods to those used above. Employing the relationship between  $\pi(d\nu|\mu)$  and the matrix  $P$ , we may write Eq. 22 as

$$\begin{bmatrix} \mu_1 \frac{\partial}{\partial x} - 1 & 0 \\ \cdot & \cdot \\ 0 & \mu_{10} \frac{\partial}{\partial x} - 1 \end{bmatrix} \begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \cdot \\ S_{\alpha\beta}(x, 10) \end{bmatrix} = -m \begin{bmatrix} P_{11} \dots P_{110} \\ \cdot \\ P_{101} \dots P_{1010} \end{bmatrix} \cdot \begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \cdot \\ S_{\alpha\beta}(x, 10) \end{bmatrix}$$

$$-m_{(2)} \begin{bmatrix} F_{\alpha\beta}(x, 1) \\ \cdot \\ F_{\alpha\beta}(x, 10) \end{bmatrix} \quad (\alpha = 1, \dots, 4, 7, \dots, 10; \beta = 1, \dots, 4, 7, \dots, 10), \quad (30)$$

where  $F_{\alpha\beta}(x, i) = \left\{ \sum_{j=1}^{10} M_{\alpha}(x, j) P_{ij} \right\} \cdot \left\{ \sum_{j=1}^{10} M_{\beta}(x, j) \cdot P_{ij} \right\} \quad (i = 1, \dots, 10).$

But, since  $\mu_5 = \mu_6 = 0$ , we can again write  $S_{\alpha\beta}(x, 5)$  and  $S_{\alpha\beta}(x, 6)$  as linear functions of  $S_{\alpha\beta}(x, i)$  ( $i = 1, \dots, 4, 7, \dots, 10$ ) and  $F_{\alpha\beta}(x, i)$  ( $i = 5, 6$ ). Then,

$$\frac{\partial}{\partial x} \begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \cdot \\ S_{\alpha\beta}(x, 4) \\ S_{\alpha\beta}(x, 7) \\ \cdot \\ S_{\alpha\beta}(x, 10) \end{bmatrix} = R \begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \cdot \\ S_{\alpha\beta}(x, 4) \\ S_{\alpha\beta}(x, 7) \\ \cdot \\ S_{\alpha\beta}(x, 10) \end{bmatrix} + \begin{bmatrix} V_{\alpha\beta}(x, 1) \\ \cdot \\ V_{\alpha\beta}(x, 4) \\ V_{\alpha\beta}(x, 7) \\ \cdot \\ V_{\alpha\beta}(x, 10) \end{bmatrix}, \quad (31)$$

where  $R$  is the same  $8 \times 8$  matrix that appeared in Eq. 25, and  $V_{\alpha\beta}(x, i)$  incorporates  $m_{(2)}$  and is a linear function of  $F_{\alpha\beta}(x, i)$ ,  $F_{\alpha\beta}(x, 5)$ , and  $F_{\alpha\beta}(x, 6)$  ( $i = 1, \dots, 4, 7, \dots, 10$ ).

Here we have a set of eight first-order, linear, nonhomogeneous differential equations. The solution is analogous to the solution of a first-order, linear, nonhomogeneous differential equation,

$$\begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \vdots \\ S_{\alpha\beta}(x, 4) \\ S_{\alpha\beta}(x, 7) \\ \vdots \\ S_{\alpha\beta}(x, 10) \end{bmatrix} = e^{R x} \cdot \underline{c} + \int_0^x e^{R(x-y)} \cdot \underline{V}_{\alpha\beta}(y) dy, \quad (32)$$

where  $\underline{V}_{\alpha\beta}(y)$  is the eight-component vector given in Eq. 31. The eight-component vector  $\underline{c}$  is determined by the boundary conditions in Eq. 23. In fact, since  $S_{\alpha\beta}(0) = \underline{c}$ , the bottom four elements of  $\underline{c}$  are zeros. The top four elements are determined using the fact that the top four elements of  $S_{\alpha\beta}(t)$  are zeros.

The covariances, variances, and correlations can then be calculated from the  $S_{\alpha\beta}$ 's and the  $M_{\alpha}$ 's by the appropriate formulas. The appendix gives the mathematical methods and details used in writing the computer program that determines the  $M_{\alpha}$ 's and the  $S_{\alpha\beta}$ 's.

#### IV. NUMERICAL RESULTS

The numerical results concerning the first- and second-moment structure of the first-passage distribution are presented in this section. First, however, is a discussion of the accuracy of the approximate model used, and of the methods used to verify that the program was coded correctly.

This model does not permit particles to take arbitrary directions of motion within the slab; only the 30 directions corresponding to the mid-points of the edges of an icosahedron are permitted. The question of the accuracy of results from this model, relative both to exact results and to results from models using different approximations, is discussed by Brockwell,<sup>3</sup> Chapter VII, Sections 5 and 6. For problems in slab geometry involving only scattering and absorption, exact solutions are possible in terms of the X- and Y-functions of Chandrasekhar.<sup>7</sup> Numerical comparisons given in Ref. 3 show that the icosahedral approximation compares favorably with the Gaussian quadrature approximation with  $n = 4$  and the spherical harmonics method with  $n = 3$ . This suggests that the icosahedral approximation should give accurate results for other cases in which the exact solutions are not known.

Internal symmetries in the model were used to verify that the coding was done correctly, that is, that the numerical output corresponds to the mathematical analysis. Considering the symmetry inherent in our model, we see that  $M_\alpha(x, \ell) = M_{11-\alpha}(t-x, 11-\ell)$  ( $0 \leq x \leq t$ ;  $\alpha = 1, \dots, 4, 7, \dots, 10$ ;  $\ell = 1, \dots, 10$ ). The output for the  $M_\alpha$ 's conditional on a particle at position  $x$  was compared with the output conditional on a particle at position  $t-x$  ( $0 \leq x \leq t$ ), and it was verified that the required symmetries did in fact hold for the numerical output. Similarly,  $S_{\alpha\beta}(x, \ell) = S_{\beta\alpha}(x, \ell)$ , and  $S_{\alpha\beta}(x, \ell) = S_{11-\alpha, 11-\beta}(t-x, 11-\ell)$  ( $\alpha = 1, \dots, 4, 7, \dots, 10$ ;  $\beta = 1, \dots, 4, 7, \dots, 10$ ;  $0 \leq x \leq t$ ;  $\ell = 1, \dots, 10$ ). The  $S_{\alpha\beta}(x, \ell)$ 's were calculated for  $\alpha = 1, \dots, 4$ ;  $\beta = 1, \dots, 4, 7, \dots, 10$ ; and  $\ell = 1, \dots, 4, 7, \dots, 10$ . The required symmetries were again satisfied by the numerical output.

#### A. Calculations of the Critical Length

We shall take the critical length  $t_c$  of a slab to be the smallest length for which the mean Eqs. 19 and 20 have no bounded nonnegative solution;  $t_c$  depends on  $m$ , the mean number of particles produced per collision, and also upon the scattering law  $\sigma(\theta)$ . (We have assumed this applies to fission products as well as to truly scattered particles; it would not be difficult to extend our method to the case where one angular distribution applies to scattered particles and another to fission-produced particles.) Now, as we increase the slab thickness (starting from  $t = 0$ ), the mean number of emergent particles  $m_{\text{tot}}$  (conditional on a single initial particle incident normally upon the slab) increases, approaching  $\infty$  as  $t \uparrow t_c$ . If  $t$  is increased slightly beyond  $t_c$ , the mean numbers of emergent particles in some directions (as calculated from Eqs. 19 and 20 become negative. Since the difference between the smallest  $t$  giving negative means and the largest  $t$  for which we can find large positive solutions of Eqs. 19 and 20 is small, we can estimate  $t_c$  fairly accurately (within the limits of the icosahedral model) from the numerical results. This was done for two scattering laws—*isotropic scattering* and *Rayleigh scattering* (the latter being used primarily to give an idea of the sensitivity of the results to deviations from isotropy).

For isotropic scattering,  $\sigma(\theta) = 1/(4\pi)$ ; therefore the directions of motion immediately after a collision are uniformly distributed over the unit sphere, and independent of the direction of motion immediately before the collision. This scattering law is often used as a reasonable approximation for neutron multiplication. For Rayleigh scattering,  $\sigma(\theta) = 3(1 + \cos^2 \theta)/(16\pi)$ . With this scattering law, particles emerging from a collision are more likely to move in a forward or backward direction than perpendicular to the direction of motion of the colliding particle. The Rayleigh scattering law is often used when studying the passage of photons through stellar atmospheres. Other scattering laws relevant to different physical situations can be analyzed without essential modification of the computer program.

Table I gives the critical length  $t_c$  for several values of  $m$  for both isotropic and Rayleigh scattering. The distance  $t_c$  is measured in units of the mean free path  $1/\lambda$ . No method is known that will give the exact value of  $t_c$  for either isotropic or Rayleigh scattering. (The method of Case<sup>6</sup> can in principle be used to give any required degree of accuracy, but the analysis becomes extremely complicated as the degree of accuracy is increased.) However, Mullikin<sup>12</sup> has given simple formulas that may be used to calculate upper and lower bounds for  $t_c$  for isotropic scattering and any value of  $m$ . A computer program was written to calculate these bounds for different  $m$ , and the results are presented in columns 4 and 5 of Table I. The final two columns of Table I present critical lengths that Case<sup>6</sup> and Mitsis<sup>8</sup> have obtained for isotropic scattering using different approximate methods. The blanks in these two columns indicate that numerical results were not reported for some values of  $m$ .

TABLE I. Dependence of the Critical Length on  $m$  (except for column 2, all results are for isotropic scattering)

m	$t_c$		Mullikin's Bounds <sup>12</sup>		Case <sup>6</sup>	Mitsis <sup>8</sup>
	Rayleigh	Isotropic	Lower	Upper		
1.05	6.589	6.605	6.553	6.684		
1.10	4.214	4.233	4.191	4.286	4.227	4.24
1.30	1.866	1.887	1.857	1.905	1.875	1.780
1.50	1.201	1.221	1.199	1.227	1.209	
1.60	1.014	1.034	1.014	1.039	1.023	1.022
1.80	0.764	0.784	0.771	0.792	0.785	
2.00	0.605	0.623	0.617	0.639	0.640	0.621
2.20	0.493	0.511	0.511	0.534		
2.40	0.411	0.429	0.434	0.459		
2.60	0.348	0.365	0.376	0.403		

Our computations of  $t_c$  for isotropic scattering fall within Mullikin's bounds for  $m \leq 2.2$ . However, for  $m > 2.2$ , our  $t_c$  is slightly below the lower bound of Mullikin. This indicates that our model should be reasonably accurate for moderate values of  $m$ , but for larger  $m$ , corresponding to smaller critical lengths, the accuracy of the approximation decreases. Comparing the critical lengths computed by Case and Mitsis, we see that Case's method gives a critical length outside Mullikin's bounds for  $m = 2.0$ . However, for smaller  $m$ , the lengths are within Mullikin's bounds. Mitsis' result for  $m = 1.3$  is outside the bounds, but the other lengths he reported are within the bounds. Since neither Case nor Mitsis presented values for  $m > 2.0$ , comparison between the approximations in this range is difficult. Case's method can, in principle, be calculated to any desired accuracy; however, the zeroth and first-order approximation for which numerical results have been given depend for their accuracy upon  $m - 1$  being small. This assumption, added to the fact that Case's critical

length for  $m = 2.0$  is outside Mullikin's bounds, while our method gives results within the bounds for  $m$  up to 2.2, suggests that our method is more accurate than Case's for  $m > 2.0$ . Mitsis' approximation is a modification of Case's and appears to be more accurate than Case's for large  $m$ . The values of  $t_c$  for Rayleigh scattering are close to, but always slightly less than, the values for isotropic scattering with the same  $m$ . The difference between the two lengths stays close to 0.018 as  $m$  varies.

## B. The Mean Number of Emergent Particles

From the numerical solution of Eqs. 19 and 20, we obtain the mean number of particles  $M_j(x, i)$  emergent in any direction  $\mu_j$ , conditional on a single initial particle with position  $x$  and direction  $\mu_i$ . In the continuous model, the mean number of particles emerging with direction cosines in  $(\mu, \mu + d\mu)$  can be written as  $f(\mu) d\mu$ , where  $f(\mu)$  is the mean density in direction  $\mu$ . The function  $f(\mu)$  can be estimated from the means  $M_j(x, i)$  in the manner described in Ref. 3, p. 99.

Thus, for example, if we consider a single particle incident normally on the right face of the slab (i.e., if we take  $x = t, \mu_i = -1$ ), then the mean density  $f(\mu)$ ,  $0 \leq \mu \leq 1$ , of the reflected particles is estimated by

$$f(1) = 3.75M_1(t, -1),$$

$$f(\mu_i) = 15M_i(t, -1), \quad i = 2, 3, 4,$$

and

$$f(0) = 0.$$

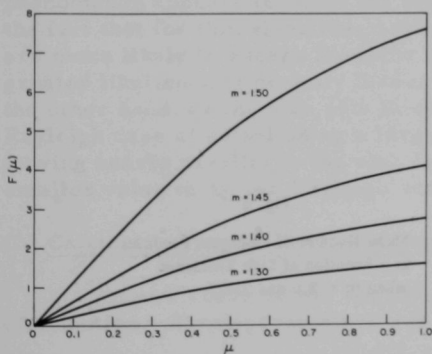


Fig. 2. The Mean Density of Particles Reflected from a Slab of Thickness 1.1 Mean Free Paths When a Single Particle Is Incident Normally on One Face

This function is illustrated in Fig. 2, where it is plotted for  $t = 1.1$  and  $m = 1.3, 1.4, 1.45$ , and  $1.50$ ; scattering is assumed to be isotropic. As  $m$  approaches the value for which the slab becomes critical ( $m \approx 1.55$ ), the mean density begins to increase rapidly.

It is of interest to know how the total number,  $m_{tot}$ , of emergent particles varies with  $t$  for fixed  $m$  and, in particular, the rate at which  $m_{tot}$  approaches  $\infty$  as  $t \uparrow t_c$ . This relationship is shown (again for a single initial particle normally incident on one slab face) for the values  $m = 1.1, 1.5, 2.0$ , and  $2.473$  in

Figs. 3, 4, and 5. The results are for

isotropic scattering; those for Rayleigh scattering are similar. Table II compares the results for Rayleigh and isotropic scattering  $m = 1.05$ . It

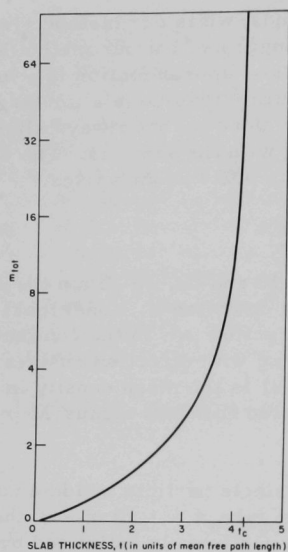


Fig. 3. Mean Number of Emergent Particles as a Function of Slab Thickness When  $m = 1.1$

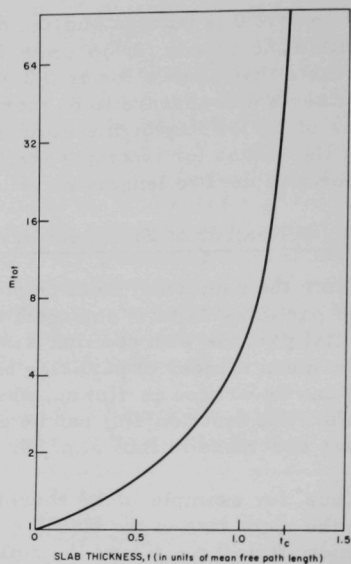


Fig. 4. Mean Number of Emergent Particles as a Function of Slab Thickness When  $m = 1.5$

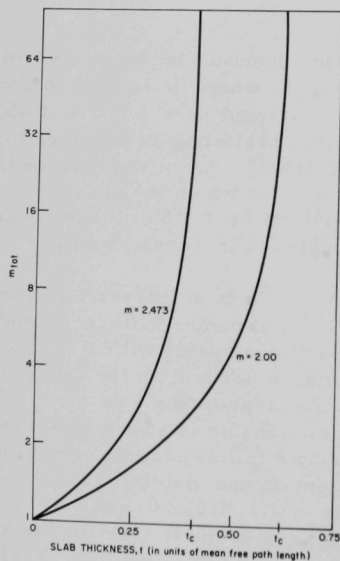


Fig. 5  
Mean Number of Emergent Particles  
as a Function of Slab Thickness  
When  $m = 2.0$  and  $2.473$



TABLE II. The Mean Number  $m_{\text{tot}}$  of Emergent Particles When the Mean Number  $m$  of Particles per Collision Is 1.05 and the Initial Particle Is Normally Incident on the Slab

Slab Thickness, $t$	Rayleigh Scattering	Isotropic Scattering	Slab Thickness, $t$	Rayleigh Scattering	Isotropic Scattering
0.1	1.006	1.006	4.3	1.940	1.943
0.3	1.020	1.020	4.5	2.068	2.069
0.5	1.036	1.037	4.7	2.221	2.221
0.7	1.054	1.056	4.9	2.409	2.407
0.9	1.075	1.077	5.1	2.645	2.639
1.1	1.097	1.101	5.3	2.952	2.941
1.3	1.122	1.126	5.5	3.369	3.350
1.5	1.149	1.153	5.7	3.970	3.935
1.7	1.178	1.182	5.9	4.916	4.849
1.9	1.210	1.214	6.1	6.630	6.482
2.1	1.244	1.248	6.3	10.702	10.249
2.3	1.280	1.285	6.5	32.992	28.389
2.5	1.320	1.325	6.55	74.04	
2.7	1.364	1.369	6.587	1,640	
2.9	1.411	1.416	6.589	15,013	
3.1	1.463	1.468	6.589+	$\infty$	
3.3	1.520	1.525	6.6		626.5
3.5	1.585	1.589	6.603		1,936
3.7	1.656	1.661	6.604		9,002
3.9	1.738	1.742	6.604+		$\infty$
4.1	1.831	1.835			

shows that for small values of  $t$ ,  $m_{\text{tot}}$  is larger for isotropic scattering, but for larger values of  $t$ ,  $m_{\text{tot}}$  is larger for Rayleigh scattering. This phenomenon appears to occur for all values of  $m$  and is probably due to the fact that for thin slabs the particles resulting from the first collision are more likely to escape from the slab in the Rayleigh case, owing to the greater likelihood of directly forward or directly backward scattering. On the other hand, as the slab gets thicker, there is more chance in the Rayleigh case of establishing a large self-sustaining population of particles moving nearly parallel to the slab faces. This would also explain the smaller value of  $t_c$  for Rayleigh scattering.

### C. Calculations of the Second Moments

We now consider the second-moment structure of the first-passage distribution. Three parameters are under consideration:

$$m \left( = \sum_{n=0}^{\infty} n\pi_n \right),$$

the mean number of particles produced per collision;



$$\sigma^2 \left( = \sum_{n=0}^{\infty} (n-m)^2 \pi_n \right),$$

the variance of the number of particles produced per collision; and  $t$ , the length of the slab. The second-moment structure varies considerably with the values of these parameters. However, the behavior is essentially the same for Rayleigh as for isotropic scattering.

Equations 30-32 show that the second factorial moments are of the form

$$S_{\alpha\beta}(x, i) = m_{(2)} w_{\alpha\beta}(x, i),$$

where, for given  $m$ ,  $w_{\alpha\beta}(x, i)$  is independent of  $\sigma^2 = m_{(2)} + m - m^2$ . The covariance of the numbers of particles emergent in directions  $\alpha$  and  $\beta$  is given by

$$\text{Cov}_{\alpha\beta}(x, i) = S_{\alpha\beta}(x, i) - M_{\alpha}(x, i)M_{\beta}(x, i), \quad \beta \neq \alpha;$$

$$\text{Cov}_{\alpha\alpha}(x, i) = S_{\alpha\alpha}(x, i) + M_{\alpha}(x, i) - M_{\alpha}(x, i)^2, \quad \beta = \alpha.$$

Hence, for fixed  $m$ ,  $t$ ,  $x$ , and  $i$ , the covariance matrix of the numbers of particles emergent in the eight possible directions of motion is a linear function of  $\sigma^2$ . (If  $m$  is not an integer,  $\sigma^2$  has a positive minimum possible value, which can easily be calculated.) In particular, the variance  $\sigma_{\text{tot}}^2$  of the total number of emergent particles is a linear function of  $\sigma^2$ ; i.e.,

$$\sigma_{\text{tot}}^2 = \xi + \eta\sigma^2,$$

where  $\xi$  and  $\eta$  depend only on  $m$ ,  $t$ ,  $x$ , and  $i$ .

To illustrate the numerical results, we shall again restrict ourselves to isotropic scattering with a single initial particle incident normally on one face of the slab. More precisely, we shall take  $x = 0$  and  $i = 1$  (recalling from Eq. 6 that  $\mu_1 = 1$ ).

If  $\pi_n = 0$  for  $n \geq 2$ , the second-moment structure of the emergent population is completely determined by the first-moment structure. In fact, the covariance of the numbers emerging in directions  $\alpha$  and  $\beta$  is expressed in terms of the means as follows:

$$\text{Cov}_{\alpha\beta} = -M_{\alpha}M_{\beta} \quad \text{if } \beta \neq \alpha;$$

$$\text{Cov}_{\alpha\alpha} = M_{\alpha} - M_{\alpha}^2 \quad \text{if } \beta = \alpha.$$

We shall therefore not discuss this case any further and assume from now on that

$$\sum_{n=2}^{\infty} \pi_n > 0.$$

A typical example of the behavior when  $m < 1$  is given by the case  $\pi_0 = 0.95$ ,  $\pi_{10} = 0.05$ , for which  $m = 0.50$ ,  $\sigma = 2.1794$ . The mean and the standard deviation of the number of transmitted particles both converge to 0 as  $t \rightarrow \infty$ ; however, the mean and the standard deviation of the number of particles reflected approach nonzero limits as  $t \rightarrow \infty$ . Figure 6 shows the

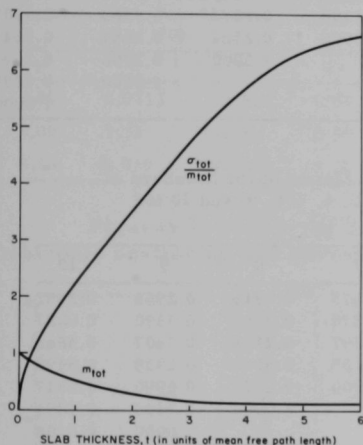


Fig. 6. The Mean and the Coefficient of Variation of the Number of Emergent Particles When  $m = 0.5$ ,  $\sigma = 2.1794$

dependence of  $m_{\text{tot}}$  and  $\sigma_{\text{tot}}/m_{\text{tot}}$  on the slab thickness,  $t$ . Note that although  $m_{\text{tot}}$  is a decreasing function of  $t$ ,  $\sigma_{\text{tot}}/m_{\text{tot}}$  increases to its asymptotic value. For  $t = 0.25$ , the correlations between emergent direction 1 and the other seven possible emergent directions are small in absolute value ( $\leq 0.10$ ) and negative; all the other correlations are positive and in the range 0.35 to 0.60. This is due to the fact that if a particle emerges in direction 1 there is some indication that no collision has occurred and hence that no other particles emerge from the slab. However, if a particle emerges traveling in a direction other than 1, then a collision must have occurred and there are probably particles emerging in different directions. For  $t = 0.50$ , the same qualitative relation exists between the correlations, although all correlations are smaller in absolute value. For larger

values of  $t$ , such as  $t = 2.5$ , all correlations are positive, although the correlations involving direction 1 are still smaller than the others; the largest element is 0.58. For the asymptotic case  $t = \infty$  (which, as far as the reflected particles are concerned, seems to be essentially reached when  $t = 4$ ), the correlations between directions 7, 8, 9, and 10 are all between 0.35 and 0.60.

We now turn to the case  $m > 1$ . The following describes the general behavior of the correlations for given  $m$  and  $\sigma$  as  $t$  increases from zero to  $t_c$ . For small  $t$ , the correlations are all positive, except for those involving direction 1, which are negative (for the reason explained in the preceding paragraph when  $m < 1$ ). As  $t$  increases, the correlations all

increase until, for some value between 0 and  $t_c$ , they are all positive. As  $t$  gets extremely close to  $t_c$ , all the correlations approach 1. To illustrate these effects, Tables III, IV, and V present the correlation matrices for isotropic scattering with  $m = 1.5$  and  $\sigma = 0.50$ ; the values of  $t$  are 0.5, 0.9, and 1.2 (the critical length  $t_c$  is 1.221).

TABLE III. Upper Half of the Correlation Matrix of the Numbers of Particles Emerging in Directions 1, 2, 3, 4, 7, 8, 9, and 10 for Slab Thickness  $t = 0.5$

	1	2	3	4	7	8	9	10
1	1.0000	-0.3524	-0.3296	-0.2969	-0.3133	-0.3412	-0.3602	-0.2100
2		1.0000	0.2942	0.2697	0.2542	0.2835	0.3037	0.1778
3			1.0000	0.2575	0.2360	0.2646	0.2844	0.1667
4				1.0000	0.2100	0.2373	0.2563	0.1505
7					1.0000	0.2524	0.2651	0.1543
8						1.0000	0.2906	0.1694
9							1.0000	0.1797
10								1.0000

TABLE IV. Upper Half of the Correlation Matrix of the Numbers of Particles Emerging in Directions 1, 2, 3, 4, 7, 8, 9, and 10 for Slab Thickness  $t = 0.9$

	1	2	3	4	7	8	9	10
1	1.0000	0.3082	0.3001	0.2849	0.2575	0.2815	0.2963	0.2352
2		1.0000	0.7532	0.7105	0.6870	0.7383	0.7690	0.6087
3			1.0000	0.6903	0.6597	0.7102	0.7407	0.5866
4				1.0000	0.6155	0.6642	0.6939	0.5498
7					1.0000	0.6771	0.6990	0.5517
8						1.0000	0.7458	0.5891
9							1.0000	0.6108
10								1.0000

TABLE V. Upper Half of the Correlation Matrix of the Numbers of Particles Emerging in Directions 1, 2, 3, 4, 7, 8, 9, and 10 for Slab Thickness  $t = 1.2$

	1	2	3	4	7	8	9	10
1	1.0000	0.9977	0.9975	0.9972	0.9970	0.9975	0.9977	0.9965
2		1.0000	0.9989	0.9985	0.9983	0.9988	0.9990	0.9978
3			1.0000	0.9983	0.9981	0.9985	0.9988	0.9976
4				1.0000	0.9977	0.9981	0.9984	0.9972
7					1.0000	0.9983	0.9985	0.9973
8						1.0000	0.9989	0.9977
9							1.0000	0.9978
10								1.0000

The close resemblance between Eqs. 19 and 20 for  $M_\alpha(x, i)$  and Eqs. 22 and 23 for  $S_{\alpha\beta}(x, i)$  suggests that the second moments become infinite for the same length  $t_c$  as the first moments. It is of interest to examine how  $\sigma_{\text{tot}}$  changes as  $m$ ,  $\sigma$ , and  $t$  vary. As discussed above,  $\sigma_{\text{tot}}^2 = \xi + \eta\sigma^2$ , where (for fixed  $x$  and  $i$ , in particular, for the values  $x = 0$ ,  $i = 1$ , under consideration)  $\xi$  and  $\eta$  depend only on  $m$  and  $t$ . The quantity  $\xi$  may be thought of as the variance due to the variability in the particle paths, and  $\eta\sigma^2$  as the variance due to the variability in the number of particles produced per collision. Table VI gives the quantities  $\xi$  and  $\eta$  for several values of  $m$  and  $t$ . (We note again that for nonintegral  $m$ , there is a smallest possible positive value of  $\sigma$ , which can easily be calculated.)

TABLE VI. Values of  $\xi$  and  $\eta$  in the Relation  $\sigma_{\text{tot}}^2 = \xi + \eta\sigma^2$  for a Single Particle Incident Normally on a Slab of Length  $t$

$m = 1.10$			$m = 1.50$			$m = 2.00$		
$t$	$\xi$	$\eta$	$t$	$\xi$	$\eta$	$t$	$\xi$	$\eta$
1.00	0.0712	2.752	0.50	1.612	3.434	0.25	3.348	2.166
3.00	7.32	102.8	0.90	39.74	65.01	0.50	212	115.5
4.15	40,010	372,180	1.20	203,700	275,230	0.60	39,456	20,050

Figures 7-9 show the relationship between  $\sigma_{\text{tot}}/m_{\text{tot}}$  and  $t$  for isotropic scattering and several values of  $m$  and  $\sigma$ . The case  $m = 2.4730$ ,

$\sigma = 1.1051$ , corresponds to a probability distribution  $\{\pi_n\}$  reported for neutron fission in  $\text{U}^{235}$ .<sup>15</sup> The graphs all show an inflection point for small values of  $t$ . The results indicate that  $\sigma_{\text{tot}}/m_{\text{tot}} \rightarrow \infty$  as  $t \uparrow t_c$ ; moreover,  $\sigma_{\text{tot}}/m_{\text{tot}}$  reaches the value 1 for  $t$  much smaller than  $t_c$ . Thus, even for a slab whose length is small compared with  $t_c$ , the variability in the number of emergent particles is quite large. This conclusion is related to the fact that, even with no multiplication of particles (i.e.,  $\pi_n = 0$  for  $n \geq 2$ ), the variance of the number of collisions experienced by emergent particles is large (c.f. Abu-Shumays<sup>1</sup> and Brockwell<sup>3</sup>).

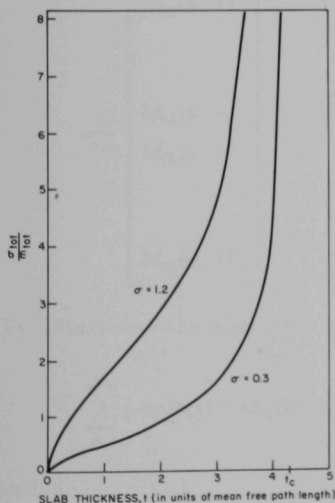


Fig. 7. The Coefficient of Variation of the Number of Emergent Particles When  $m = 1.1$

The graphs corresponding to those in Figs. 7-9 for Rayleigh scattering are similar to the curves for isotropic scattering and are not shown. Of course,  $\sigma_{\text{tot}}/m_{\text{tot}} \rightarrow \infty$  in this case as  $t \uparrow t_c$  for Rayleigh scattering, not the value of  $t_c$  for isotropic scattering. The similarity of the two sets of curves indicates that the behavior of  $\sigma_{\text{tot}}/m_{\text{tot}}$  is insensitive to small changes in the scattering law.

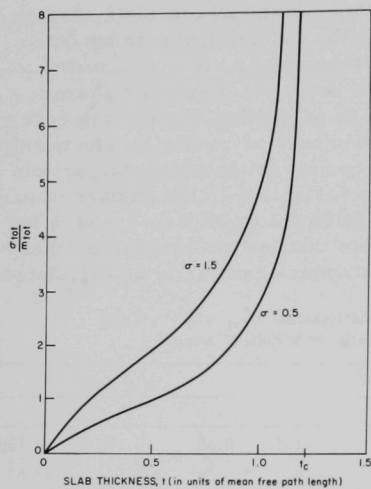


Fig. 8. The Coefficient of Variation of the Number of Emergent Particles When  $m = 1.5$

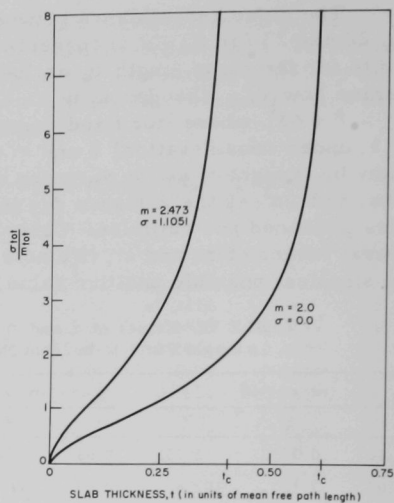


Fig. 9. The Coefficient of Variation of the Number of Emergent Particles When  $m = 2.0$  and  $2.473$

## APPENDIX A

Mathematical Methods Used in the Computer Program

This appendix presents in detail the mathematical methods used in the computer program to calculate the formulas for the means and the second factorial moments; these formulas were given in Eqs. 26 and 32.

First we discuss the computation of  $M_{\alpha}(x, i)$ , the mean number of particles emergent in direction  $\alpha$  ( $\alpha = 1, \dots, 4, 7, \dots, 10$ ) conditional on a particle at position  $x$  ( $0 \leq x \leq t$ ) traveling in direction  $i$  ( $i = 1, \dots, 10$ ). We return to the basic Eq. 24; i.e.,

$$\begin{bmatrix} \mu_1 \frac{\partial}{\partial x} & 0 \\ & \ddots \\ 0 & \mu_{10} \frac{\partial}{\partial x} \end{bmatrix} \begin{bmatrix} M_{\alpha}(x, 1) \\ \vdots \\ M_{\alpha}(x, 10) \end{bmatrix} = \begin{bmatrix} 1-mP_{1,1} & -mP_{1,2} & \dots & -mP_{1,10} \\ \vdots & \vdots & \ddots & \vdots \\ -mP_{10,1} & \dots & 1-mP_{10,10} \end{bmatrix} \begin{bmatrix} M_{\alpha}(x, 1) \\ \vdots \\ M_{\alpha}(x, 10) \end{bmatrix}.$$

Since  $\mu_5 = \mu_6 = 0$ , we can rewrite this as Eq. 25,

$$\frac{\partial}{\partial x} \begin{bmatrix} M_{\alpha}(x, 1) \\ \vdots \\ M_{\alpha}(x, 4) \\ M_{\alpha}(x, 7) \\ \vdots \\ M_{\alpha}(x, 10) \end{bmatrix} = R \begin{bmatrix} M_{\alpha}(x, 1) \\ \vdots \\ M_{\alpha}(x, 4) \\ M_{\alpha}(x, 7) \\ \vdots \\ M_{\alpha}(x, 10) \end{bmatrix}.$$

To determine the elements of the  $8 \times 8$  matrix  $R$ , we use the equations

$$\sum_{j=1}^{10} (-mP_{5j}) \cdot M_{\alpha}(x, j) + M_{\alpha}(x, 5) = 0 \quad (\text{A.1})$$

and

$$\sum_{j=1}^{10} (-mP_{6j}) \cdot M_{\alpha}(x, j) + M_{\alpha}(x, 6) = 0 \quad (\alpha = 1, \dots, 4, 7, \dots, 10). \quad (\text{A.2})$$

Therefore,

$$M_{\alpha}(x, 5) = \sum_{\substack{j=1 \\ j \neq 5,6}}^{10} M_{\alpha}(x, j) \left\{ \frac{mP_{5j}(1 - mP_{66}) + mP_{56}mP_{6j}}{(1 - mP_{55})(1 - mP_{66}) - mP_{56}mP_{65}} \right\} \quad (A.3)$$

and

$$M_{\alpha}(x, 6) = \sum_{\substack{j=1 \\ j \neq 5,6}}^{10} M_{\alpha}(x, j) \left\{ \frac{mP_{6j}(1 - mP_{55}) + mP_{65}mP_{5j}}{(1 - mP_{55})(1 - mP_{66}) - mP_{56}mP_{65}} \right\} \quad (A.4)$$

( $\alpha = 1, \dots, 4, 7, \dots, 10$ ).

So  $r_{ij}$ , the  $(i, j)$ th element of  $R$ , is given by

$$r_{ij} = \frac{-mP_{ij} - mP_{i5} \cdot \gamma_5(j) - mP_{i6} \cdot \gamma_6(j)}{\mu_i}$$

( $i = 1, \dots, 4, j = 1, \dots, 4, i \neq j$ ; for  $i = 5, \dots, 8$  and  $j = 5, \dots, 8$ ,  $i$  and  $j$  are replaced on the right-hand side of this equation by  $i+2$  and  $j+2$ .)

(A-5)

$$r_{ii} = \frac{1 - mP_{ii} - mP_{i5} \cdot \gamma_5(i) - mP_{i6} \cdot \gamma_6(i)}{\mu_i}$$

( $i = 1, \dots, 4$ ; for  $i = 5, \dots, 8$ ,  $i$  is replaced by  $i+2$  on the right-hand side),

where

$$\gamma_5(j) = \frac{mP_{5j}(1 - mP_{66}) + mP_{56}mP_{6j}}{(1 - mP_{55})(1 - mP_{66}) - mP_{56}mP_{65}} \quad (A.6)$$

and

$$\gamma_6(j) = \frac{mP_{6j}(1 - mP_{55}) + mP_{65}mP_{5j}}{(1 - mP_{55})(1 - mP_{66}) - mP_{56}mP_{65}} \quad (j = 1, \dots, 4, 7, \dots, 10). \quad (A.7)$$

To calculate  $\exp(Rt)$  as required in Eq. 26, we use the Jordan decomposition of the matrix  $R$ . If  $m$ , the mean number of particles produced per collision, is not equal to 1, then the eight eigenvalues of  $R$  will in

general be distinct; in fact, from a certain symmetry of  $R$ , one can show that these eigenvalues form four pairs of numbers with opposite signs. However, if  $m = 1$ , zero is a double eigenvalue of  $R$ ; this double eigenvalue causes the Jordan decomposition of  $R$  to be nondiagonal. Since this nondiagonality complicates the computations, we exclude the case  $m = 1$ . If, in fact, numerical results are desired for  $m = 1$ , we can perform the calculations for  $m = 1.0001$  and  $m = 0.9999$  and average the results, provided the slab is not nearly critical when  $m = 1.0001$ . (For  $m = 1.0001$  and  $m = 0.9999$ , there will be two eigenvalues close to zero; experience with the numerical routine JACOBI, used to calculate eigenvalues and eigenvectors, has indicated that it can separate these two nonzero eigenvalues for these  $m$ , so that the diagonal Jordan decomposition can be achieved numerically.)

Thus, letting  $T = [t_1 \dots t_8]$  be the matrix of eigenvectors of  $R$ , we have

$$T^{-1} R T = \begin{bmatrix} \lambda_1 & 0 \\ & \ddots \\ 0 & \lambda_8 \end{bmatrix}, \quad (\text{A.8})$$

where  $\lambda_1, \dots, \lambda_8$  are the eight distinct eigenvalues of  $R$ . The matrices  $T$ ,  $T^{-1}$ , and the numbers  $\lambda_1, \dots, \lambda_8$  may be complex. (It seems that if  $m < 1$ , all eight eigenvalues, and thus the eigenvectors, are real; however, if  $m > 1$ , there is always one pair of purely imaginary eigenvalues. There are then six real eigenvectors and two other eigenvectors, complex conjugates of each other, with imaginary parts.)

Since

$$\exp(Rt) = I + \sum_{j=1}^{\infty} (Rt)^j / j!,$$

it follows that

$$T^{-1} \exp(Rt) T = I + T^{-1} R t T + T^{-1} (Rt)^2 T / 2! + \dots$$

In terms of the matrix

$$\Lambda = \begin{bmatrix} \lambda_1 & 0 \\ & \ddots \\ 0 & \lambda_8 \end{bmatrix},$$



we can write

$$T^{-1} \exp(Rt)T = I + \Delta t + (\Delta t)(\Delta t)/2! + \dots = \exp(\Delta t);$$

therefore,

$$\exp(Rt) = T \exp(\Delta t)T^{-1}. \quad (\text{A.9})$$

Letting

$$T^{-1} = \begin{bmatrix} \tilde{x}_1 \\ \cdot \\ \cdot \\ \cdot \\ \cdot \\ \cdot \\ \cdot \\ \tilde{x}_8 \end{bmatrix},$$

we have

$$\exp(Rx) = e^{\lambda_1 x} U_1 + \dots + e^{\lambda_8 x} U_8, \quad (\text{A.10})$$

where

$$U_i = \tilde{t}_i \cdot \tilde{x}_i \quad (i=1, \dots, 8). \quad (\text{A.11})$$

Each  $U_i$  is an  $8 \times 8$  matrix, since  $\tilde{t}_i$  is a column vector and  $\tilde{x}_i$  is a row vector. The eight matrices  $U_i$  are computed.

Now let  $M(x)$  be the  $8 \times 8$  matrix

$$\begin{bmatrix} M_1(x, 1) & \dots & M_4(x, 1) & M_7(x, 1) & \dots & M_{10}(x, 1) \\ \cdot & & & & & \cdot \\ \cdot & & & & & \cdot \\ \cdot & & & & & \cdot \\ M_1(x, 4) & & & & & \\ M_1(x, 7) & & & & & \\ \cdot & & & & & \\ \cdot & & & & & \\ \cdot & & & & & \\ M_1(x, 10) & \dots & & & & M_{10}(x, 10) \end{bmatrix}.$$

Then  $M(t) = \exp(Rt) \cdot M(0)$ , where  $M(0)$  is the  $8 \times 8$  matrix determined by the boundary conditions. This matrix was partitioned as

$$\begin{bmatrix} C_1 & C_2 \\ 0 & I \end{bmatrix},$$

and the solutions for  $C_1$  and  $C_2$  were given after Eq. 29. Thus  $M(x) = e^{\lambda_1 x} Z_1 + \dots + e^{\lambda_8 x} Z_8$  ( $0 \leq x \leq t$ ), where  $Z_i = U_i \cdot M(0)$  ( $i = 1, \dots, 8$ ). The eight matrices  $Z_i$  are calculated. Now we use the fact that  $M_\alpha(x, 5)$  and  $M_\alpha(x, 6)$  are linear combinations of the  $M_\alpha(x, j)$  ( $j = 1, \dots, 4, 7, \dots, 10$ ;  $\alpha = 1, \dots, 4, 7, \dots, 10$ ) as given in Eqs. A.3 and A.4. Thus, if we let  $M(x)$  be the  $10 \times 8$  matrix

$$\begin{bmatrix} M_1(x, 1) & \dots & M_4(x, 1) & M_7(\lambda, 1) & \dots & M_{10}(x, 1) \\ \vdots & & & & & \vdots \\ M_1(x, 10) & \dots & M_4(x, 10) & M_7(x, 10) & \dots & M_{10}(x, 10) \end{bmatrix}. \quad (\text{A.12})$$

then  $M(x) = e^{\lambda_1 x} W_1 + \dots + e^{\lambda_8 x} W_8$ , where the  $W_i$  are all  $10 \times 8$  matrices, and

$$\left. \begin{aligned} W_q(i, j) &= Z_q(i, j) & (i = 1, \dots, 4; j = 1, \dots, 8), \\ W_q(i+2, j) &= Z_q(i, j) & (i = 5, \dots, 8; j = 1, \dots, 8), \\ W_q(5, j) &= \sum_{k=1}^4 \gamma_5(k) Z_q(k, j) + \sum_{k=5}^8 \gamma_5(k+2) Z_q(k, j) & (j = 1, \dots, 8), \\ W_q(6, j) &= \sum_{k=1}^4 \gamma_6(k) Z_q(k, j) + \sum_{k=5}^8 \gamma_6(k+2) Z_q(k, j) & (j = 1, \dots, 8) \\ & & (q = 1, \dots, 8), \end{aligned} \right\} (\text{A.13})$$

and  $\gamma_5(k), \gamma_6(k)$  are defined by Eqs. A.6 and A.7. The eight matrices  $W$  are computed. These matrices completely determine the  $10 \times 8$  matrix  $M(x)$ , which gives the mean number of particles emergent in each of the eight possible emergent directions for a particle at position  $x$  traveling in each of the 10 possible directions of motion. The eight  $W$ 's, eight  $U$ 's and eight  $\lambda$ 's are all stored for use in the second part of the program.

Now we consider Eq. 30, the basic equation for the second factorial moments:

$$\begin{bmatrix} \mu_1 \frac{\partial}{\partial x} & 0 \\ & \ddots \\ 0 & \mu_{10} \frac{\partial}{\partial x} \end{bmatrix} \begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \vdots \\ S_{\alpha\beta}(x, 10) \end{bmatrix} = \begin{bmatrix} 1 - mP_{1,1} & -mP_{1,2} & \dots & -mP_{1,10} \\ \vdots & \vdots & \ddots & \vdots \\ -mP_{10,1} & \dots & \dots & 1 - mP_{10,10} \end{bmatrix} \begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \vdots \\ S_{\alpha\beta}(x, 10) \end{bmatrix}$$

$$\cdot e^{-m(2)} \begin{bmatrix} F_{\alpha\beta}(x, 1) \\ \vdots \\ F_{\alpha\beta}(x, 10) \end{bmatrix}.$$

We recall that

$$F_{\alpha\beta}(x, \ell) = \left\{ \sum_{k=1}^{10} M_{\alpha}(x, k) P_{\ell k} \right\} \cdot \left\{ \sum_{k=1}^{10} M_{\beta}(x, k) P_{\ell k} \right\}$$

$$(\alpha = 1, \dots, 4, 7, \dots, 10; \beta = 1, \dots, 4, 7, \dots, 10; \ell = 1, \dots, 10).$$

The first factor can be thought of as the  $\ell$ th row of the matrix  $P$  multiplied by the column vector  $M_{\alpha}(x)$ ; writing  $M_{\alpha}(x, \ell)$  in terms of the  $W$ 's, we get

$$F_{\alpha\beta}(x, \ell) = \left\{ \sum_{k=1}^{10} P_{\ell k} \sum_{q=1}^8 e^{\lambda_q x} W_q(k, \alpha) \right\} \cdot \left\{ \sum_{m=1}^{10} P_{\ell m} \sum_{r=1}^8 e^{\lambda_r x} W_r(m, \beta) \right\}$$

$$(\alpha = 1, \dots, 4, \beta = 1, \dots, 4, \ell = 1, \dots, 10; \text{ for } \alpha \text{ and } \beta = 7, \dots, 10, \alpha \text{ and } \beta \text{ are replaced by } \alpha - 2 \text{ and } \beta - 2 \text{ on the right-hand side}).$$

This equation can be written

$$F_{\alpha\beta}(x, \ell) = \sum_{q=1}^8 \sum_{r=1}^8 e^{(\lambda_q + \lambda_r)x} \cdot X_{\alpha\beta qr}(\ell), \quad (\text{A.14})$$

where

$$X_{\alpha\beta qr}(\ell) = \sum_{k=1}^{10} P_{\ell k} W_q(k, \alpha) \cdot \sum_{m=1}^{10} P_{\ell m} W_r(m, \beta)$$

( $\alpha = 1, \dots, 4$ ,  $\beta = 1, \dots, 4$ ,  $\ell = 1, \dots, 10$ ; for  $\alpha$  and  $\beta = 7, \dots, 10$ ,  
 $\alpha - 2$  and  $\beta - 2$  replace  $\alpha$  and  $\beta$  on the right side). (A.15)

The X's are calculated.

Next we change the form of the basic equation to that of Eq. 31, i.e.,

$$\frac{\partial}{\partial x} \begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \vdots \\ S_{\alpha\beta}(x, 4) \\ S_{\alpha\beta}(x, 7) \\ \vdots \\ S_{\alpha\beta}(x, 10) \end{bmatrix} = R \begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \vdots \\ S_{\alpha\beta}(x, 4) \\ S_{\alpha\beta}(x, 7) \\ \vdots \\ S_{\alpha\beta}(x, 10) \end{bmatrix} + \begin{bmatrix} V_{\alpha\beta}(x, 1) \\ \vdots \\ \vdots \\ \vdots \\ \vdots \\ V_{\alpha\beta}(x, 8) \end{bmatrix}.$$

by using the fact that  $\mu_5 = \mu_6 = 0$ . The  $8 \times 8$  matrix  $R$  is the same as in Eq. A.5, and elementary algebra shows that

$$V_{\alpha\beta}(x, \ell) = \left[ F_{\alpha\beta}(x, \ell) + \frac{mP_{\ell 5}(1 - mP_{66}) + mP_{\ell 6}mP_{65}}{(1 - mP_{55})(1 - mP_{66}) - mP_{56}mP_{65}} F_{\alpha\beta}(x, 5) \right. \\ \left. + \frac{mP_{\ell 6}(1 - mP_{55}) + mP_{\ell 5}mP_{56}}{(1 - mP_{55})(1 - mP_{66}) - mP_{56}mP_{65}} F_{\alpha\beta}(x, 6) \right] \frac{-m(2)}{\mu_\ell}$$

( $\alpha = 1, \dots, 4$ ,  $\beta = 1, \dots, 4$ ,  $\ell = 1, \dots, 4$ ; similar equations hold for  
 $\alpha = 7, \dots, 10$ ,  $\beta = 7, \dots, 10$ , and  $\ell = 5, \dots, 8$ ). (A.16)

This can be simplified to

$$V_{\alpha\beta}(x, \ell) = \sum_{q=1}^8 \sum_{r=1}^8 e^{(\lambda_q + \lambda_r)x} \cdot Y_{\alpha\beta qr}(\ell), \quad (A.17)$$

where

$$Y_{\alpha\beta qr}(\ell) = \left\{ X_{\alpha\beta qr}(\ell) + K_5(\ell) \cdot X_{\alpha\beta qr}(5) + K_6(\ell) \cdot X_{\alpha\beta qr}(6) \right\} \frac{-m(\ell)}{\mu_\ell}$$

$(\alpha = 1, \dots, 4, \dots, 7, \dots, 10, \beta = 1, \dots, 4, \dots, 7, \dots, 10, \ell = 1, \dots, 4;$   
 for  $\ell = 5, \dots, 8$ , the  $\ell$  in  $X$  and in  $\mu_\ell$  is replaced by  $\ell + 2$ )

(A.18)

and

$$K_5(\ell) = \frac{mP_{\ell 5}(1 - mP_{66}) + mP_{\ell 6}mP_{65}}{(1 - mP_{55})(1 - mP_{66}) - mP_{56}mP_{65}}$$

$(\ell = 1, \dots, 4; \text{ for } \ell = 5, \dots, 8, \ell \text{ is replaced by } \ell + 2),$

(A.19)

$$K_6(\ell) = \frac{mP_{\ell 6}(1 - mP_{55}) + mP_{\ell 5}mP_{56}}{(1 - mP_{55})(1 - mP_{66}) - mP_{56}mP_{65}}$$

$(\ell = 1, \dots, 4; \text{ for } \ell = 5, \dots, 8, \ell \text{ is replaced by } \ell + 2).$

(A.20)

The  $K$ 's and the  $Y$ 's are computed. Now the solution is

$$\begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \vdots \\ S_{\alpha\beta}(x, 4) \\ S_{\alpha\beta}(x, 7) \\ \vdots \\ S_{\alpha\beta}(x, 10) \end{bmatrix} = \exp(Rx) \left\{ \underline{z}_{\alpha\beta} + \int_0^x \exp(-yR) \sum_{q=1}^8 \sum_{r=1}^8 Y_{\alpha\beta qr} \cdot e^{(\lambda_q + \lambda_r)y} dy \right\}.$$
(A.21)

Next we write  $\exp(-yR)$  as

$$\sum_{s=1}^8 e^{-\lambda_s y} U_s.$$

Then the integral in Eq. A.21 can be written as

$$\sum_{s=1}^8 \sum_{q=1}^8 \sum_{r=1}^8 U_s \cdot Y_{\alpha\beta qr} \cdot \int_0^x e^{(\lambda_q + \lambda_r - \lambda_s)y} dy.$$
(A.22)

Now the reason for breaking up

$$\int_0^x \exp(-yR) \cdot Y_{\alpha\beta}(y) dy$$

into the triple summation of Eq. A.22 is apparent, since

$$\int_0^x e^{(\lambda_q + \lambda_r - \lambda_s)y} dy$$

can be integrated analytically. Therefore the solution is

$$\begin{bmatrix} S_{\alpha\beta}(x, 1) \\ \vdots \\ S_{\alpha\beta}(x, 4) \\ S_{\alpha\beta}(x, 7) \\ \vdots \\ S_{\alpha\beta}(x, 10) \end{bmatrix} = \exp(xR) \left\{ \varpi_{\alpha\beta} + \sum_{s=1}^8 \sum_{q=1}^8 \sum_{r=1}^8 U_s \cdot Y_{\alpha\beta qr} \cdot \left[ \frac{e^{(\lambda_q + \lambda_r - \lambda_s)x} - 1}{\lambda_q + \lambda_r - \lambda_s} \right] \right\}. \quad (A.23)$$

assuming  $\lambda_q + \lambda_r - \lambda_s \neq 0$  ( $s=1, \dots, 8$ ;  $q=1, \dots, 8$ ;  $r=1, \dots, 8$ ); the eight-component vector  $\varpi_{\alpha\beta}$  is determined by the boundary conditions. Since  $S_{\alpha\beta}(0) = \varpi_{\alpha\beta}$ , the bottom four components of  $\varpi_{\alpha\beta}$  are zeros.

The symmetry of directions 1, ..., 4 with directions 10, ..., 7 shows that the  $S_{\alpha\beta}$ 's need only be calculated for  $\alpha = 1, \dots, 4$  and  $\beta = 1, \dots, 4, 7, \dots, 10$ ; the symmetry relations are  $S_{\alpha\beta}(x, \ell) = S_{11-\alpha, 11-\beta}(t-x, 11-\ell)$  and  $S_{\alpha\beta}(x, \ell) = S_{\beta\alpha}(x, \ell)$  ( $\alpha = 1, \dots, 4, 7, \dots, 10$ ;  $\beta = 1, \dots, 4, 7, \dots, 10$ ;  $\ell = 1, \dots, 4$ ;  $0 \leq x \leq t$ ). Thus a complete solution is obtained by evaluating  $S_{\alpha\beta}(x, \ell)$  for  $\alpha = 1, \dots, 4$ ,  $\beta = 1, \dots, 4, 7, \dots, 10$ , and  $\ell = 1, \dots, 4, 7, \dots, 10$  ( $0 \leq x \leq t$ ). Let  $S(x)$  be the  $8 \times 32$  matrix

$$\begin{bmatrix} S_{11}(x, 1) \dots S_{14}(x, 1) S_{17}(x, 1) \dots S_{1,10}(x, 1) S_{21}(x, 1) \dots S_{2,10}(x, 1) S_{31}(x, 1) \dots S_{4,10}(x, 1) \\ \vdots \\ S_{11}(x, 4) \\ S_{11}(x, 7) \\ \vdots \\ S_{11}(x, 10) \dots \end{bmatrix} S_{4,10}(x, 10) \quad (A.24)$$

and let  $\begin{bmatrix} \text{Int1}(x) \\ \text{Int2}(x) \end{bmatrix}$  be the  $8 \times 32$  matrix

$$[\text{Int}_{1,1}(x) \text{Int}_{1,2}(x) \dots \text{Int}_{1,4}(x) \text{Int}_{1,7}(x) \dots \text{Int}_{1,10}(x) \text{Int}_{2,1}(x) \dots \text{Int}_{2,10}(x)],$$

where  $\text{Int}_{\alpha\beta}(x)$  is the eight-component column vector

$$\sum_{s=1}^6 \sum_{q=1}^8 \sum_{r=1}^8 U_s \cdot Y_{\alpha\beta qr} \cdot \left[ \frac{e^{(\lambda_q + \lambda_r - \lambda_s)x} - 1}{\lambda_q + \lambda_r - \lambda_s} \right]. \quad (\text{A.25})$$

Thus  $\text{Int1}(x)$  and  $\text{Int2}(x)$  are each  $4 \times 32$  matrices. Finally, let  $C$  be the  $4 \times 32$  matrix

$$[\xi_{11} \dots \xi_{14} \xi_{17} \dots \xi_{1,10} \xi_{21} \dots \xi_{4,10}],$$

where the  $\xi_{\alpha\beta}$ 's are the top four (i.e., nonzero) components of the  $\xi_{\alpha\beta}$ 's used in Eq. A.23.

Then we have the equation

$$S(x) = \exp(Rx) \left\{ \begin{bmatrix} C \\ 0 \end{bmatrix} + \begin{bmatrix} \text{Int1}(x) \\ \text{Int2}(x) \end{bmatrix} \right\}. \quad (\text{A.26})$$

To compute  $C$ , we use the boundary conditions on  $S(t)$ ; i.e.,  $S_{\alpha\beta}(t, \ell) = 0$  ( $\alpha = 1, \dots, 4$ ,  $\beta = 1, \dots, 4, 7, \dots, 10$ ,  $\ell = 1, \dots, 4$ ). Thus we compute

$$\begin{bmatrix} \text{Int1}(t) \\ \text{Int2}(t) \end{bmatrix}$$

using Eq. A.25. Then letting

$$\exp(Rt) = \begin{bmatrix} E_{11} & E_{12} \\ E_{21} & E_{22} \end{bmatrix},$$

we have

$$0 = E_{11} \cdot [C + \text{Int1}(t)] + E_{12}[\text{Int2}(t)]. \quad (\text{A.27})$$

Therefore,  $C = -E_{11}^{-1}E_{12} \text{Int2}(t) - \text{Int1}(t)$ . The  $4 \times 32$  matrix  $C$  is computed using this formula. Then  $S(x)$  can be calculated for arbitrary  $x$  ( $0 \leq x \leq t$ ) using Eqs. A.26 and A.25.

The transformations from the second factorial moments  $S$  to the more meaningful variances, covariances, correlations, and standard deviations are then made using the standard formulas.

It has been observed that the method of calculation becomes numerically unstable when  $t$  gets very close to the critical length  $t_c$  ( $t_c - t \approx 0.001$ ). A similar phenomenon occurred in the nonmultiplicative case (Brockwell<sup>3</sup>) when  $t$  becomes large (approximately seven mean free paths). However, in the nonmultiplicative case, the range of accuracy was increased considerably by considering thick slabs to be superpositions of thinner slabs (see Ref. 3, Chapter VI, Section 5). An analogous approach could be used to study thick slabs in the multiplicative case, but so far this approach has not been investigated.



# APPENDIX B Listing of Computer Program

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LEVEL 15 ( 1 JAN 68)                                OS/360  FORTRAN H  DATE  68.261/22.11.32
COMPILER OPTIONS - NAME=  MAIN,OPT=00,LINECNT=57,SOURCE,EBCDIC,NOLIST,NODECK,
C                                                         LOAD,MAP,NOEDIT,IO,NXXREF
C
C      STOCHASTIC TRANSPORT PROGRAM II
C
ISN 0002      IMPLICIT REAL*8(A-H,O-Z)
ISN 0003      REAL*8 LENGTH,M,M2,MU,KAPPA5,KAPPA6
ISN 0004      COMPLEX*16  COMP, CR, CT, CTEMP, CTINV, D, DETERM, E11,
1  E12, FACTOR, INT, INT1, INT2, MEAN, SCONST, SMOP, THETA,
2  U, VTEMP, W, XTEMP1, XTEMP2, XX, Y, Z
ISN 0005      DIMENSION  B2(4), COMP(10,10), CONST(8,8), CORR(8,8),
1  CR(8,8), CT(8,8), CTEMP(8,8), CTINV(8,8), D(4,4), E11(4,4),
2  E12(4,4), GAM5(10), GAM6(10), INT(8,32), INT1(4,32),
3  INT2(4,32), KAPPA5(10), KAPPA6(10), MEAN(10,8), MU(10),
4  OCOV(8,32), OMEAN(10,8), P(10,10), R(8,8), RR(8,8),
5  RSC(8,32), SCAT(9), SCONST(8,32), SDEV(8), SML(4,32),
6  SMOP(8,32), T(8,8), THETA(8), U(8,8,8), VAR(4,8), VTEMP(8),
7  W(8,10,8), XX(4,8,8,10), Y(4,8,8,8,8), Z(8,8,8)
ISN 0006      FIVE = 5.0
ISN 0007      MU(1) = 1.0
ISN 0008      MU(2) = (DSQRT(FIVE) + 1.0)/4.0
ISN 0009      MU(3) = 0.5
ISN 0010      MU(4) = (DSQRT(FIVE) - 1.0)/4.0
ISN 0011      MU(5) = C.0
ISN 0012      DO 102 I = 1,5
ISN 0013      102 MU(11-I) = -MU(1)
ISN 0014      READ (5,902) ISCAT
ISN 0015      IF (ISCAT) 103,106,108
C
C      IF ISCAT = 0, ISOTROPIC SCATTERING; IF ISCAT = -1, RAYLEIGH
C      SCATTERING; IF ISCAT = +1, A DIFFERENT SCATTERING LAW IS READ IN.
C
ISN 0016      103 SCAT(1) = 0.050
ISN 0017      SCAT(2) = (11.0 + DSQRT(FIVE))/320.0
ISN 0018      SCAT(3) = 1.0/32.0
ISN 0019      SCAT(4) = (11.0 - DSQRT(FIVE))/320.0
ISN 0020      SCAT(5) = 0.0250
ISN 0021      DO 104 I = 6,9
ISN 0022      104 SCAT(I) = SCAT(10-I)
ISN 0023      WRITE (6,835)
ISN 0024      GO TO 109
ISN 0025      106 DO 107 I=1,9
ISN 0026      107 SCAT(I) = 1.0/30.0
ISN 0027      WRITE (6,837)
ISN 0028      GO TO 109
ISN 0029      108 READ (5,900) (SCAT(I),I=1,9)
ISN 0030      109 CONTINUE
C
C      COMPUTATION OF MATRIX P
C
ISN 0031      P(1,1) = SCAT(1)
ISN 0032      P(1,2) = 4.0*SCAT(2)
ISN 0033      P(1,3) = 4.0*SCAT(3)
ISN 0034      P(1,4) = 4.0*SCAT(4)
ISN 0035      P(2,1) = SCAT(2)
ISN 0036      P(2,2) = SCAT(1) + SCAT(2) + SCAT(3) + SCAT(4)
ISN 0037      P(2,3) = SCAT(2) + SCAT(3) + SCAT(4) + SCAT(5)
ISN 0038      P(2,4) = SCAT(2) + SCAT(3) + SCAT(5) + SCAT(6)
ISN 0039      P(3,1) = SCAT(3)
ISN 0040      P(3,2) = P(2,3)
ISN 0041      P(3,3) = SCAT(1) + SCAT(2) + SCAT(6) + SCAT(7)
ISN 0042      P(3,4) = SCAT(2) + SCAT(4) + SCAT(5) + SCAT(7)
ISN 0043      P(4,1) = SCAT(4)
ISN 0044      P(4,2) = P(2,4)
ISN 0045      P(4,3) = P(3,4)

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ISN 0046      P(4,4) = SCAT(1) + SCAT(3) + SCAT(6) + SCAT(8)
ISN 0047      DO 110 I=7,10
ISN 0048      DO 110 J=7,10
ISN 0049      110 P(I,J) = P(11-I,11-J)
ISN 0050      P(7,1) = SCAT(6)
ISN 0051      P(7,2) = SCAT(4) + SCAT(5) + SCAT(7) + SCAT(8)
ISN 0052      P(7,3) = SCAT(3) + SCAT(5) + SCAT(6) + SCAT(8)
ISN 0053      P(7,4) = SCAT(2) + SCAT(4) + SCAT(7) + SCAT(9)
ISN 0054      P(8,1) = SCAT(7)
ISN 0055      P(8,2) = SCAT(5) + SCAT(6) + SCAT(7) + SCAT(8)
ISN 0056      P(8,3) = SCAT(3) + SCAT(8) + SCAT(4) + SCAT(9)
ISN 0057      P(8,4) = SCAT(3) + SCAT(5) + SCAT(6) + SCAT(8)
ISN 0058      P(9,1) = SCAT(8)
ISN 0059      P(9,2) = SCAT(6) + SCAT(7) + SCAT(8) + SCAT(9)
ISN 0060      P(9,3) = SCAT(5) + SCAT(6) + SCAT(7) + SCAT(8)
ISN 0061      P(9,4) = SCAT(4) + SCAT(5) + SCAT(7) + SCAT(8)
ISN 0062      P(10,1) = SCAT(9)
ISN 0063      P(10,2) = 4.0*SCAT(8)
ISN 0064      P(10,3) = 4.0*SCAT(7)
ISN 0065      P(10,4) = 4.0*SCAT(6)
ISN 0066      DO 115 I=1,4
ISN 0067      DO 115 J=7,10
ISN 0068      115 P(I,J) = P(11-I,11-J)
ISN 0069      P(5,1) = SCAT(5)
ISN 0070      P(5,2) = 2.0*SCAT(4) + 2.0*SCAT(6)
ISN 0071      P(5,3) = 2.0*SCAT(2) + 2.0*SCAT(8)
ISN 0072      P(5,4) = 2.0*SCAT(3) + 2.0*SCAT(7)
ISN 0073      P(6,1) = SCAT(5)
ISN 0074      P(6,2) = 2.0*SCAT(3) + 2.0*SCAT(7)
ISN 0075      P(6,3) = 2.0*SCAT(4) + 2.0*SCAT(6)
ISN 0076      P(6,4) = 2.0*SCAT(2) + 2.0*SCAT(8)
ISN 0077      DO 120 I=5,6
ISN 0078      DO 120 J=7,10
ISN 0079      120 P(I,J) = P(11-I,J)
ISN 0080      P(1,5) = 2.0*SCAT(5)
ISN 0081      P(1,6) = P(1,5)
ISN 0082      P(2,5) = SCAT(4) + SCAT(6)
ISN 0083      P(2,6) = SCAT(3) + SCAT(7)
ISN 0084      P(3,5) = SCAT(2) + SCAT(8)
ISN 0085      P(3,6) = SCAT(4) + SCAT(6)
ISN 0086      P(4,5) = SCAT(3) + SCAT(7)
ISN 0087      P(4,6) = SCAT(2) + SCAT(8)
ISN 0088      P(5,5) = SCAT(1) + SCAT(9)
ISN 0089      P(5,6) = 2.0*SCAT(5)
ISN 0090      P(6,5) = P(5,6)
ISN 0091      P(6,6) = P(5,5)
ISN 0092      DO 125 I=7,10
ISN 0093      DO 125 J=5,6
ISN 0094      125 P(I,J) = P(11-I,J)
ISN 0095      WRITE (6,905)
ISN 0096      WRITE (6,910) ((P(I,J),J=1,10),I=1,10)

C
C      READ IN M,M2, AND NUMBER OF LENGTHS FOR THIS MEAN
C
ISN 0097      130 READ (5,880) M,M2,NUMLTH
ISN 0098      IF (M .LE. 0.0) GO TO 500

C
C      COMPUTATION OF MATRIX R
C
ISN 0100      DEN = (M*P(5,5) - 1.0) *(M*P(6,6) - 1.0) - (M*P(6,5))*(M*P(5,6))
ISN 0101      DO 140 I=1,4
ISN 0102      GAM6(I) = ((M*P(6,5))*(M*P(5,I)) - (M*P(6,I))*(M*P(5,5)-1.0))/DEN
ISN 0103      GAM6(I+6) = ((M*P(6,5))*(M*P(5,I+6)) - (M*P(6,I+6))*(M*P(5,5)-1.0)
1/DEN
ISN 0104      GAM5(I) = ((M*P(5,6))*(M*P(6,I)) - (M*P(5,I))*(M*P(6,6)-1.0))/DEN
ISN 0105      GAM5(I+6) = (M*P(5,6)*(M*P(6,I+6)) - (M*P(5,I+6))*(M*P(6,6)-1.0)
1/DEN
ISN 0106      140 CONTINUE
ISN 0107      DO 150 I=1,4
ISN 0108      DO 150 J=1,4
ISN 0109      R(I,J) = (-M*P(I,J) - M*P(I,5)*GAM5(J) - M*P(I,6)*GAM6(J))/MU(I)

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ISN 0110      R(I,J+4) = (-M*P(I,J+6) - M*P(I,5)*GAM5(J+6) - M*P(I,6)*GAM6(J+6))
              1/MU(I)
ISN 0111      R(I+4,J) = (-M*P(I+6,J) - M*P(I+6,5)*GAM5(J) - M*P(I+6,6)*GAM6(J))/
              1/MU(I+6)
ISN 0112      R(I+4,J+4) = (-M*P(I+6,J+6) - M*P(I+6,5)*GAM5(J+6) - M*P(I+6,6)*GAM6
              1(J+6))/MU(I+6)
ISN 0113      150 CONTINUE
ISN 0114      DO 155 I= 1,4
ISN 0115      R(I,1) = R(I,1) + (1.C/MU(I))
ISN 0116      R(I+4,1+4) = R(I+4,1+4) + (1.0/MU(I+6))
ISN 0117      155 CONTINUE
ISN 0118      WRITE (6,915)
ISN 0119      WRITE (6,975) ((R(I,J),J=1,8),I=1,8)
ISN 0120      DO 170 I=1,8
ISN 0121      DO 170 J=1,8
ISN 0122      170 RR(I,J) = R(I,J)

```

C  
C  
C      COMPUTATION OF EIGENVALUES & EIGENVECTORS

```

ISN 0123      KONST = 1
ISN 0124      CALL CLOCK(T1)
ISN 0125      CALL JACOBI (RR,T,8,KONST,8)
ISN 0126      CALL CLOCK(T2)
ISN 0127      TT = T2 - T1
ISN 0128      WRITE (6,945) KONST,TT
ISN 0129      WRITE (6,950)
ISN 0130      WRITE (6,965) ((RR(I,J),J=1,8),I=1,8)
ISN 0131      WRITE (6,960)
ISN 0132      WRITE (6,965) ((T(I,J),J=1,8),I=1,8)
ISN 0133      IDUM = 0
ISN 0134      DO 180 I=1,7
ISN 0135      IF (IDUM.NE.1) GO TO 171
ISN 0137      IDUM = 0
ISN 0138      GO TO 180
ISN 0139      171 IF (DABS(RR(I,1+1)) .GE. 1.0D-07) GO TO 174
ISN 0141      THETA(I) = RR(I,1)
ISN 0142      DO 172 J=1,8
ISN 0143      172 CT(J,I) = T(J,1)
ISN 0144      GO TO 180
ISN 0145      174 IF (DABS(RR(I,1)) .LE. 1.0D-07) GO TO 175
ISN 0147      THETA(I) = RR(I,1)
ISN 0148      THETA(I) = THETA(I) + (0.0,1.0)*RR(I,1+1)
ISN 0149      THETA(I+1) = RR(I+1,1+1)
ISN 0150      THETA(I+1) = THETA(I+1) + (0.0,1.0)*RR(I+1,I)
ISN 0151      GO TO 176
ISN 0152      175 THETA(I) = RR(I,1+1)*(0.0,1.0)
ISN 0153      THETA(I+1) = RR(I+1,I)*(0.0,1.0)
ISN 0154      176 DO 178 J=1,8
ISN 0155      CT(J,I) = T(J,1)
ISN 0156      CT(J,I) = CT(J,I) + (0.0,1.0)*T(J,I+1)
ISN 0157      CT(J,I+1) = T(J,I)
ISN 0158      178 CT(J,I+1) = CT(J,I+1) - (0.0,1.0)*T(J,I+1)
ISN 0159      IDUM = 1
ISN 0160      180 CONTINUE
ISN 0161      IF (DABS(RR(7,8)) .GE. 1.0D-07) GO TO 183
ISN 0163      THETA(8) = RR(8,8)
ISN 0164      DO 182 J=1,8
ISN 0165      182 CT(J,8) = T(J,8)
ISN 0166      183 DO 184 I=1,8
ISN 0167      DO 184 J=1,8
ISN 0168      184 CTINV(I,J) = CT(I,J)
ISN 0169      WRITE (6,955)
ISN 0170      WRITE (6,908) (THETA(I),I=1,8)

```

C  
C  
C      CHECK OF DIAGONALIZATION, AND COMPUTATION OF THE 8 U'S

```

ISN 0171      CALL MATINV(CTINV,8,SDEV,0,DETERM,8)
ISN 0172      WRITE (6,960)
ISN 0173      WRITE (6,964) ((CT(I,J),J=1,8),I=1,8)
ISN 0174      WRITE (6,970)
ISN 0175      WRITE (6,964) ((CTINV(I,J),J=1,8),I=1,8)

```

```

ISN 0176      DO 185 I=1,8
ISN 0177      DO 185 J=1,8
ISN 0178      185 CR(I,J) = R(I,J)
ISN 0179      CALL CMTMLT (CTINV,8,8,CR,8,8,CTEMP)
ISN 0180      CALL CMTMLT (CTEMP,8,8,CT,8,8,CR)
ISN 0181      WRITE (6,920)
ISN 0182      WRITE (6,964) ((CR(I,J),J=1,8),I=1,8)
ISN 0183      DO 187 I=1,8
ISN 0184      DO 187 J=1,8
ISN 0185      DO 187 K=1,8
ISN 0186      187 U(I,J,K) = CT(J,I)*CTINV(I,K)

C
C      READ IN (NUMLTH) LENGTHS FOR THIS MEAN
C

ISN 0187      KCOUNT = 0
ISN 0188      190 READ (5,900) LENGTH
ISN 0189      KCOUNT = KCOUNT + 1
ISN 0190      WRITE (6,918) LENGTH

C
C      CALCULATION OF EXP(R*LENGTH)
C

ISN 0191      DO 195 I=1,8
ISN 0192      DO 195 J=1,8
ISN 0193      195 CR(I,J) = 0.0
ISN 0194      DO 200 K=1,8
ISN 0195      FACTOR = CDEXP(THETA(K)*LENGTH)
ISN 0196      DO 200 I=1,8
ISN 0197      DO 200 J=1,8
ISN 0198      200 CR(I,J) = CR(I,J) + U(K,I,J)*FACTOR
ISN 0199      WRITE (6,985)
ISN 0200      WRITE (6,964) ((CR(I,J),J=1,8),I=1,8)

C
C      CALCULATION OF EXP(R*LENGTH) USING H. G. SUBROUTINE
C

ISN 0201      CALL EXMATR(R,T,LENGTH,8,CORR,CONST,SDEV)
ISN 0202      WRITE (6,986)
ISN 0203      WRITE (6,975) ((T(I,J), J=1,8),I=1,8)

C
C      CALCULATION OF CONSTANTS MATRIX
C

ISN 0204      209 DO 210 I=1,4
ISN 0205      DO 210 J=1,4
ISN 0206      REAL = CR(I,J)
ISN 0207      E11(I,J) = REAL
ISN 0208      REAL = CR(I,J+4)
ISN 0209      E12(I,J) = REAL
ISN 0210      CONST(I+4,J) = 0.0
ISN 0211      210 CONST(I+4,J+4) = 0.0
ISN 0212      DO 215 I=5,8
ISN 0213      215 CONST(I,I) = 1.0
ISN 0214      CALL MATINV (E11,4,8,2,0,DETERM,4)
ISN 0215      WRITE (6,946) DETERM
ISN 0216      WRITE (6,964) ((E11(I,J),J=1,4),I=1,4)
ISN 0217      DO 220 I=1,4
ISN 0218      DO 220 J=1,4
ISN 0219      220 CONST(I,J) = E11(I,J)
ISN 0220      CALL CMTMLT (E11,4,4,E12,4,4,0)
ISN 0221      DO 225 I=1,4
ISN 0222      DO 225 J=1,4
ISN 0223      225 CONST(I,J+4) = -D(I,J)
ISN 0224      WRITE (6,990)
ISN 0225      WRITE (6,965) ((CONST(I,J),J=1,8),I=1,8)

C
C      CALCULATION OF MATRICES Z'S AND W'S
C

ISN 0226      DO 240 I=1,8
ISN 0227      DO 240 J=1,8
ISN 0228      DO 240 K=1,8
ISN 0229      Z(I,J,K) = 0.0
ISN 0230      DO 240 L=1,8
ISN 0231      240 Z(I,J,K) = Z(I,J,K) + U(I,J,L)*CONST(L,K)

```

```

ISN 0232      DO 275 N1=1,8
ISN 0233      DO 270 J=1,8
ISN 0234      DO 250 I=1,4
ISN 0235      250 W(N1,I,J) = Z(N1,I,J)
ISN 0236      DO 255 I=5,8
ISN 0237      255 W(N1,I+2,J) = Z(N1,I,J)
ISN 0238      W(N1,5,J) = 0.0
ISN 0239      W(N1,6,J) = 0.0
ISN 0240      DO 260 L=1,4
ISN 0241      W(N1,5,J) = W(N1,5,J) + GAM5(L)*Z(N1,L,J)
ISN 0242      260 W(N1,6,J) = W(N1,6,J) + GAM6(L)*Z(N1,L,J)
ISN 0243      DO 265 L=5,8
ISN 0244      W(N1,5,J) = W(N1,5,J) + GAM5(L+2)*Z(N1,L,J)
ISN 0245      265 W(N1,6,J) = W(N1,6,J) + GAM6(L+2)*Z(N1,L,J)
ISN 0246      270 CONTINUE
ISN 0247      275 CONTINUE
ISN 0248      280 READ (5,930) X
ISN 0249      IF (X) 285,290,290

C
C      CALCULATION OF MEAN MATRIX
C
ISN 0250      290 DO 292 I=1,10
ISN 0251      DO 292 J=1,8
ISN 0252      MEAN(I,J) = 0.0
ISN 0253      DO 292 K=1,8
ISN 0254      292 MEAN(I,J) = MEAN(I,J) + (CDEXP(THETA(K)*X))*W(K,I,J)
ISN 0255      WRITE (6,935) LENGTH,X
ISN 0256      WRITE (6,937) M
ISN 0257      DO 293 I=1,10
ISN 0258      DO 293 J=1,8
ISN 0259      293 OMEAN(I,J) = MEAN(I,J)
ISN 0260      WRITE (6,940)
ISN 0261      WRITE (6,965) ((OMEAN(I,J), J=1,8),I=1,10)
ISN 0262      296 DO 297 I=1,10
ISN 0263      DO 297 J=1,8
ISN 0264      297 OMEAN(I,J) = (0.0,-1.0)*MEAN(I,J)
ISN 0265      WRITE (6,967)
ISN 0266      WRITE (6,965) ((OMEAN(I,J), J=1,8),I=1,10)
ISN 0267      GO TO 280

C
C      CALCULATION OF SECOND FACTORIAL MOMENTS
C      FIRST, CALCULATION OF X'S
C
ISN 0268      285 CONTINUE
ISN 0269      STDEV = DSQRT(M2 + M - M*M)
ISN 0270      WRITE (6,840) M,STDEV
ISN 0271      DO 308 I = 1,10
ISN 0272      DO 308 J = 1,10
ISN 0273      308 COMP(I,J) = P(I,J)
ISN 0274      DO 310 IALPHA = 1,4
ISN 0275      DO 310 IBETA = 1,8
ISN 0276      DO 310 IQ = 1,8
ISN 0277      DO 310 IR = 1,8
ISN 0278      DO 310 IL = 1,10
ISN 0279      XTEMP1 = 0.0
ISN 0280      XTEMP2 = 0.0
ISN 0281      DO 305 IK = 1,10
ISN 0282      XTEMP1 = XTEMP1 + COMP(IL,IK)*W(IQ,IK,IALPHA)
ISN 0283      305 XTEMP2 = XTEMP2 + COMP(IL,IK)*W(IR,IK,IBETA)
ISN 0284      310 XX(IALPHA,IBETA,IQ,IR,IL) = XTEMP1*XTEMP2
ISN 0285      DO 320 L=1,4
ISN 0286      KAPPA5(L) = (M*P(L,5)*(1.0-M*P(6,6)) + M*P(L,6)*M*P(6,5))/DEN
ISN 0287      320 KAPPA6(L) = (M*P(L,5)*M*P(5,6) + M*P(L,6)*(1.0-M*P(5,5)))/DEN
ISN 0288      DO 325 L = 5,8
ISN 0289      KAPPA5(L) = (M*P(L+2,5)*(1.0 - M*P(6,6)) + M*P(L+2,6)*M*P(6,5))/DEN
ISN 0290      325 KAPPA6(L) = (M*P(L+2,5)*M*P(5,6) + M*P(L+2,6)*(1.0-M*P(5,5)))/DEN

C
C      CALCULATION OF Y'S
C
ISN 0291      RMM2 = -M2

```

```

ISN 0292      DO 335 IALPHA = 1,4
ISN 0293      DO 335 IBETA = 1,8
ISN 0294      DO 335 IQ = 1,8
ISN 0295      DO 335 IR = 1,8
ISN 0296      DO 335 IL = 1,4
ISN 0297      Y(IALPHA,IBETA,IQ,IR,IL) = (XX(IALPHA,IBETA,IQ,IR,IL) + KAPPA5(IL)
1*XX(IALPHA,IBETA,IQ,IR,5) + KAPPA6(IL)*XX(IALPHA,IBETA,IQ,IR,6))*
2(RMM2/MU(IL))
ISN 0298      335 Y(IALPHA,IBETA,IQ,IR,IL+4) = (XX(IALPHA,IBETA,IQ,IR,IL+6) + KAPPA5
1(IL + 4)*XX(IALPHA,IBETA,IQ,IR,5) + KAPPA6(IL + 4)*XX(IALPHA,IBETA
2,IQ,IR,6))*(RMM2/MU(IL+6))

C
C      CALCULATION OF INTEGRALS
C
ISN 0299      DO 345 IALPHA = 1,4
ISN 0300      DO 345 IBETA = 1,8
ISN 0301      DO 336 IM = 1,8
ISN 0302      336 INT(IM,8*(IALPHA-1) + IBETA) = 0.0
ISN 0303      DO 345 IS = 1,8
ISN 0304      DO 337 IM = 1,8
ISN 0305      337 VTEMP(IM) = 0.0
ISN 0306      DO 340 IQ = 1,8
ISN 0307      DO 340 IR = 1,8
ISN 0308      FACTOR = (CDEXP((THETA(IQ) + THETA(IR) - THETA(IS))*LENGTH) - 1.0)
1/(THETA(IQ) + THETA(IR) - THETA(IS))
ISN 0309      DO 340 IM = 1,8
ISN 0310      340 VTEMP(IM) = VTEMP(IM) + Y(IALPHA,IBETA,IQ,IR,IM)*FACTOR
ISN 0311      DO 344 IL = 1,8
ISN 0312      DO 344 IM = 1,8
ISN 0313      344 INT(IL,8*(IALPHA-1) + IBETA) = INT(IL,8*(IALPHA-1) + IBETA) +
1U(IS,IL,IM)*VTEMP(IM)
ISN 0314      345 CONTINUE

C
C      CALCULATION OF CONSTANTS MATRIX
C
ISN 0315      DO 347 I = 1,4
ISN 0316      DO 347 J = 1,32
ISN 0317      347 INT2(I,J) = INT(I + 4,J)
ISN 0318      DO 350 I = 1,8
ISN 0319      DO 350 J = 1,8
ISN 0320      350 CR(I,J) = 0.0
ISN 0321      DO 352 K = 1,8
ISN 0322      FACTOR = CDEXP(THETA(K)*LENGTH)
ISN 0323      DO 352 I = 1,8
ISN 0324      DO 352 J = 1,8
ISN 0325      352 CR(I,J) = CR(I,J) + U(K,I,J)*FACTOR
ISN 0326      DO 355 I = 1,4
ISN 0327      DO 355 J = 1,4
ISN 0328      E11(I,J) = CR(I,J)
ISN 0329      355 E12(I,J) = CR(I,J+4)
ISN 0330      CALL CMTMLT (E12,4,4,INT2,4,32,INT1)
ISN 0331      CALL MATINV (E11,4,82,0,DETERM,4)
ISN 0332      CALL CMTMLT ( E11,4,4,INT1,4,32,INT2)
ISN 0333      DO 360 I = 1,4
ISN 0334      DO 360 J = 1,32
ISN 0335      SCONST(I+4,J) = 0.0
ISN 0336      360 SCONST(I,J) = -INT2(I,J) - INT(I,J)
ISN 0337      DO 362 I = 1,8
ISN 0338      DO 362 J = 1,32
ISN 0339      362 RSC(I,J) = SCONST(I,J)
ISN 0340      WRITE (6,1005)
ISN 0341      WRITE (6,1010) ((RSC(I,J), J=1,32),I=1,8)
ISN 0342      DO 365 I=1,8
ISN 0343      DO 365 J=1,32
ISN 0344      365 OCOV(I,J) = (0.0,-1.0)*SCONST(I,J)
ISN 0345      WRITE (6,1020)
ISN 0346      WRITE (6,1010) ((OCOV(I,J), J=1,32),I=1,8)

C
C      CALCULATIONS FOR ARBITRARY X
C
ISN 0347      370 READ (5,930) X

```

```

ISN 0348      IF (X) 450,375,375
ISN 0349 375 DO 385 IALPHA = 1,4
ISN 0350      DO 385 IBETA = 1,8
ISN 0351      DO 376 IM = 1,8
ISN 0352 376 INT(IM,8*((IALPHA-1) + IBETA)) = 0.0
ISN 0353      DO 385 IS = 1,8
ISN 0354      DO 377 IM = 1,8
ISN 0355 377 VTEMP(IM) = 0.0
ISN 0356      DO 380 IQ = 1,8
ISN 0357      DO 380 IR = 1,8
ISN 0358      FACTOR = (CDEXP((THETA(IQ) + THETA(IR) - THETA(IS))*X) - 1.0)/(THE
      1TA(IQ) + THETA(IR) - THETA(IS))
      DO 380 IM = 1,8
ISN 0359 380 VTEMP(IM) = VTEMP(IM) + Y(IALPHA,IBETA,IQ,IR,IM)*FACTOR
ISN 0360      DO 384 IL = 1,8
ISN 0361      DO 384 IM = 1,8
ISN 0362 384 INT(IL,8*((IALPHA-1) + IBETA)) = INT(IL,8*((IALPHA-1) + IBETA) +
ISN 0363      1U(IS,IL,IM)*VTEMP(IM)
ISN 0364 385 CONTINUE
ISN 0365      DO 390 I = 1,4
ISN 0366      DO 390 J = 1,32
ISN 0367 390 INT(I,J) = INT(I,J) + SCONST(I,J)
ISN 0368      DO 400 I = 1,8
ISN 0369      DO 400 J = 1,8
ISN 0370 400 CR(I,J) = 0.0
ISN 0371      DO 405 K = 1,8
ISN 0372      FACTOR = CUEXP(THETA(K)*X)
ISN 0373      DO 405 I = 1,8
ISN 0374      DO 405 J = 1,8
ISN 0375 405 CR(I,J) = CR(I,J) + U(K,I,J)*FACTOR
ISN 0376      CALL CMTMLT(CR,8,8,INT,8,32,SMOP)
ISN 0377      WRITE (6,1015) X
ISN 0378      DO 410 I=1,8
ISN 0379      DO 410 J=1,32
ISN 0380 410 OCOV(I,J) = SMOP(I,J)
ISN 0381      WRITE (6,1010) ((OCOV(I,J), J=1,32), I=1,8)
ISN 0382      IF (LENGTH .NE. X) GO TO 414
ISN 0383      DO 412 I=1,4
ISN 0384      DO 412 J=1,32
ISN 0385 412 SML(I,J) = OCOV(I+4,J)
ISN 0386 414 DO 415 I=1,8
ISN 0387      DO 415 J=1,32
ISN 0388 415 OCOV(I,J) = (0.0,-1.0)*SMOP(I,J)
ISN 0389      WRITE (6,1025)
ISN 0390      WRITE (6,1010) ((OCOV(I,J), J=1,32),I=1,8)
ISN 0391      GO TO 370
ISN 0392

```

C  
C  
C

# CALCULATION OF VARIANCES AND CORRELATIONS

```

ISN 0393 450 DO 455 I=1,4
ISN 0394      DO 455 J=1,4
ISN 0395      VAR(I,J) = RSC(I,9*J - 8) + CONST(I,J)*(1.0-CONST(I,J))
ISN 0396 455 VAR(I,J+4) = SML(5-I,37 - 9*J) + CONST(I,J+4)*(1.0-CONST(I,J+4))
ISN 0397      WRITE (6,925) ((VAR(I,J),J=1,8),I=1,4)
ISN 0398      DO 470 I=1,4
ISN 0399      DO 460 IALPHA = 1,4
ISN 0400      IALP1 = IALPHA + 1
ISN 0401      DO 460 IBETA = IALP1,8
ISN 0402 460 CORR(IALPHA,IBETA) = (RSC(I,8*((IALPHA-1) + IBETA) -
      1 CONST(I,IALPHA)*CONST(I,IBETA))/DSQRT(VAR(I,IALPHA)*VAR(I,IBETA))
      DO 465 IALPHA = 5,7
ISN 0403      IALP1 = IALPHA + 1
ISN 0404      DO 465 IBETA = IALP1,8
ISN 0405 465 CORR(IALPHA,IBETA) = (SML(5-I,73 - 8*IALPHA - IBETA) -
ISN 0406      1CONST(I,IALPHA)*CONST(I,IBETA))/DSQRT(VAR(I,IALPHA)*VAR(I,IBETA))
      DO 467 J=1,8
ISN 0407 467 CORR(J,J) = 1.0
ISN 0408      DO 468 I1=2,8
ISN 0409      I1M1 = I1 - 1
ISN 0410      DO 468 J1 = 1,I1M1
ISN 0411 468 CORR(I1,J1) = CORR(J1,I1)
ISN 0412

```



```

ISN 0413      WRITE (6,805) I
ISN 0414      WRITE (6,810) (VAR(I,J), J=1,8)
ISN 0415      DO 469 J1=1,8
ISN 0416      469 SDEV(J1) = DSQRT(VAR(I,J1))
ISN 0417      WRITE (6,820)
ISN 0418      WRITE (6,922) (CONST(I,J1), J1=1,8)
ISN 0419      WRITE (6,922) (SDEV(J1), J1=1,8)
ISN 0420      WRITE (6,815)
ISN 0421      WRITE (6,922) ((CORR(I1,J1),J1=1,8),I1=1,8)
ISN 0422      IF (I .NE. 1) GO TO 470
ISN 0424      DO 4690 I1 = 1,8
ISN 0425      DO 4690 J1 = 1,8
ISN 0426      4690 CORR(I1,J1) = CORR(I1,J1)*DSQRT(VAR(I,I1)*VAR(I,J1))
ISN 0427      WRITE (6,1030)
ISN 0428      WRITE (6,922) ((CORR(I1,J1), J1=1,8),I1=1,8)
ISN 0429      SUM1 = 0.0
ISN 0430      SUM2 = 0.0
ISN 0431      SUM3 = 0.0
ISN 0432      DO 4692 I1 = 1,4
ISN 0433      DO 4692 J1 = 1,4
ISN 0434      SUM1 = SUM1 + CORR(I1,J1)
ISN 0435      SUM2 = SUM2 + CORR(I1 + 4,J1 + 4)
ISN 0436      4692 SUM3 = SUM3 + CORR(I1,J1+4)
ISN 0437      SUM = SUM1 + SUM2 + 2.0*SUM3
ISN 0438      SR = 0.0
ISN 0439      ST = 0.0
ISN 0440      DO 4694 J1 = 1,4
ISN 0441      ST = ST + CONST(I,J1)
ISN 0442      4694 SR = SR + CONST(I,J1 + 4)
ISN 0443      SP = SR + ST
ISN 0444      SUM1 = DSQRT(SUM1)
ISN 0445      SUM2 = DSQRT(SUM2)
ISN 0446      SUM = DSQRT(SUM)
ISN 0447      WRITE (6,1040) LENGTH,M,STDEV
ISN 0448      WRITE (6,1035) I,SR,SUM2,ST,SUM1,SP,SUM
ISN 0449      470 CONTINUE
ISN 0450      IF (KCOUNT .EQ. NUMLTH) GO TO 130
ISN 0452      GO TO 190
ISN 0453      500 STOP
ISN 0454      805 FORMAT (////,25X,'VARIANCES AND CORRELATIONS FOR PARTICLES WITH IN
      1TIAL DIRECTION',I3)
ISN 0455      810 FORMAT (/ ,25X,'VARIANCES FOR PARTICLES EMERGING IN DIRECTIONS 1-4
      1 AND 7-10',/,5X,8D14.7,/)
ISN 0456      815 FORMAT (/ ,25X,'CORRELATION MATRIX',/)
ISN 0457      820 FORMAT (26X,'MEANS AND STANDARD DEVIATIONS FOR PARTICLES WITH THIS
      1 INITIAL DIRECTION',/,26X,'EMERGENT DIRECTIONS ARE 1-4 AND 7-10,
      2WITH MEANS DIRECTLY ABOVE THE STANDARD DEVIATIONS',/)
ISN 0458      835 FORMAT (1H0,4CX,'RAYLEIGH SCATTERING',/)
ISN 0459      837 FORMAT (1H0,4CX,'ISOTROPIC SCATTERING',/)
ISN 0460      840 FORMAT (1H0,5X,'MEAN NUMBER OF PARTICLES PRODUCED PER COLLISION IS
      1',F10.5,'STANDARD DEVIATION IS',F10.5,/)
ISN 0461      880 FORMAT (10X,2F10.8,I3)
ISN 0462      900 FORMAT (10X,5F10.8)
ISN 0463      902 FORMAT (I3)
ISN 0464      905 FORMAT (1H1,40X,'MATRIX OF PROBABILITIES P(I,J)')
ISN 0465      908 FORMAT (40X,G16.4)
ISN 0466      910 FORMAT (10X,10F12.8)
ISN 0467      915 FORMAT (40X,'MATRIX R')
ISN 0468      918 FORMAT (40X,'LENGTH IS',F10.5)
ISN 0469      920 FORMAT (40X,'CHECK MATRIX')
ISN 0470      922 FORMAT (2X,8F16.7)
ISN 0471      925 FORMAT (10X,8D14.7)
ISN 0472      930 FORMAT (F8.4)
ISN 0473      935 FORMAT (1H1,10X,'MEAN MATRIX FOR TOTAL LENGTH =',F5.2,' WITH PARTI
      1CLE AT POSITION X =',F5.2/)
ISN 0474      937 FORMAT (10X,'MEAN NUMBER OF PARTICLES PRODUCED PER COLLISION IS',
      1F8.4,/)
ISN 0475      940 FORMAT (10X,'ROW I REPRESENTS PARTICLE PRESENTLY TRAVELLING IN ITH
      1 DIRECTION. COLUMN J REPRESENTS PARTICLE EMERGING IN DIRECTION J'
      2/)
ISN 0476      945 FORMAT (20X,'NO. OF ITERATIONS =',I3,' TIME(MS) =',F8.0)

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ISN 0477      946 FORMAT (40X,'DETERMINANT IS',2D16.7,/)
ISN 0478      950 FORMAT (40X,'RETURNED MATRIX WITH EIGENVALUES'//)
ISN 0479      955 FORMAT (40X,'THETAS')
ISN 0480      960 FORMAT (40X,'EIGENVECTOR COLUMN MATRIX'//)
ISN 0481      964 FORMAT (2X,8D16.7//2X,8D16.7,/)
ISN 0482      965 FORMAT (2X,8D16.7,/)
ISN 0483      967 FORMAT (1H0,10X,'IMAGINARY PART OF MEAN MATRIX.  SHOULD BE ZERO'//)
ISN 0484      970 FORMAT (40X,'INVERSE MATRIX OF EIGENVECTORS'//)
ISN 0485      975 FORMAT (2X,8F16.7,/)
ISN 0486      985 FORMAT (40X,'EXP(R*LENGTH)')
ISN 0487      986 FORMAT (40X,'EXP(R*LENGTH) USING H. G. SUBROUTINE'//)
ISN 0488      990 FORMAT (40X, 'CONSTANTS MATRIX'//)
ISN 0489      1005 FORMAT (1H1,5X,'CONSTANT MATRIX FOR SECOND FACTORIAL MOMENTS.  PAR
                1TICLE AT 0,  1-TH ROW GIVES INITIAL DIRECTION 1-4, 7-10.',/5X,'(AL
                2PHA,BETA)-TH MOMENT IN COL. 8(ALPHA-1) + BETA, ALPHA = 1 TO 4 AND
                3BETA = 1 TO 4 AND (7 TO 10).')

ISN 0490      1010 FORMAT (4(2X,8D16.7//),/)
ISN 0491      1015 FORMAT (10X,'SECOND MOMENT OUTPUT, X = ',F8.4/)
ISN 0492      1020 FORMAT (1H0,20X,'IMAGINARY PART OF CONSTANTS MATRIX.  SHOULD BE ZE
                1RO.',/)

ISN 0493      1025 FORMAT (//,20X,'IMAGINARY PART OF SECOND FACTORIAL MOMENT OUTPUT.
                1 SHOULD BE ZERO.',//)

ISN 0494      1030 FORMAT (//,20X,'VARIANCE-COVARIANCE MATRIX FOR PARTICLE INCIDENT A
                1T X = 0 TRAVELLING IN DIRECTION 1',//)

ISN 0495      1035 FORMAT (//,20X,'FOR PARTICLE AT X = 0 WITH INITIAL DIRECTION',I3,/
                1,9X,'THE MEAN NUMBER OF PARTICLES REFLECTED IS',I2X,F16.7,' WITH S
                2TANDARD DEVIATION',F16.7,/,9X,'THE MEAN NUMBER OF PARTICLES TRANSM
                3ITTED IS',I0X,F16.7,' WITH STANDARD DEVIATION',F16.7,/,9X,'THE MEA
                4N OF THE TOTAL NUMBER OF PARTICLES PRODUCED IS',F16.7,' WITH STAND
                5ARD DEVIATION',F16.7,//)

ISN 0496      1040 FORMAT (//,20X,'THE LENGTH OF THE SLAB IS',F10.4,/,20X,'THE MEAN NUM
                1BER OF PARTICLES PRODUCED PER COLLISION IS',F10.4,' WITH STANDARD
                2DEVIATION',F10.4)

ISN 0497      END

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